Mumford Road
County Highway No 24
Troy Township

23

FIELD BOOK

307 T

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURTHOUSE
CHARDON, O.
PHONE 250-X

Book 23

MUMFORD RD. #24 SEC. A-B-C-D-E-F-G-H
Slopes & culverts 2-39

GROVE RD #211 SEC. D (pt) (PARKMAN TWP)
Align't & loc. of structures 41-53
GROVE RD #211 SEC. D (pt) (TROY TWP.)
Align't & loc. of structures 54

MUMFORD RD #24 SEC. B (pt)
Levels 55-56

GEORGIA #124 RD. SEC. B Bridge 66-67

Agler (#210) E. end (Parkmin Twp) 57

7/7/29 — J. Richey, C. Rand, G. Grismold

New BM 33	3.27	1124.15			1120.88
			10.20	1113.95	
	3.43	1117.00	10.58	1113.57	
34			4.03	1112.97	Grade changed
35			3.47	1113.53	Grade changed
36			1.34	1115.66	
	13.11	1129.99	0.12	1116.88	
37			10.27	1119.72	
38			6.66	1123.33	
39			4.37	1125.62	
	8.10	1134.27	3.82	1126.17	
40			7.02	1127.25	
41			5.39	1128.88	
	4.92	1137.79	1.40	1132.87	
New BM			1.48	1136.39	

C2.0 / 26.7	C1.4 / 25.7			F4.2 / 22.5	F4.7 / 23.3
F2.9 / 21.3	F3.1 / 20.3			F2.5 / 19.9	F2.8 / 20.9
F1.7 / 21.2	F2.3 / 20.2			F2.1 / 20.5	F2.3 / 21.5
F1.1 / 22.2	F1.6 / 21.2			F3.4 / 21.0	F3.4 / 22.0
F2.3 / 21.2	F2.3 / 20.2	special R.		30P	C7.6 / 31.8
F2.3 / 20.5	F2.7 / 19.5	"	R	300	C6.6 / 31.3
F1.0 / 23.0	F1.1 / 22.0	"	R	390	C7.2 / 31.0
F3.0 / 22.0	F3.4 / 21.0	"	R	290	C5.6 / 30.0
F3.2 / 23.0	F4.0 / 22.0			F2.2 / 20.3	F2.0 / 21.3

MUMFORD RD.

			7/15/29	Richey Caufield Hoffman Guan.	
BM#5	7.37	1180.31			1172.94
	11.29	1191.01	0.59	1179.72	
58			8.73	1182.28	
59			5.87	1185.14	
60			3.01	1188.00	
	9.15	1197.89	2.27	1188.74	
61			7.39	1190.50	
62			4.89	1193.00	
63			2.39	1195.50	
	9.80	1206.68	1.01	1196.88	
64			8.68	1198.00	
65			6.18	1200.50	
66			3.68	1203.00	
BM#6	0.88	1206.71	0.88	1205.80	1205.83
	7.58	1212.12	2.17	1204.54	
67			6.62	1205.50	
68			4.55	1207.57	
69			2.48	1209.64	

F1.4 / 22.2	F1.6 / 21.2	F0.8 / 22.4	F0.7 / 23.4
C0.2 / 24.9	C0.2 / 22.9	C0.0 / 23.6	C0.2 / 24.6
C0.7 / 25.3	C0.5 / 24.3	C0.6 / 24.5	C0.8 / 25.5
C0.2 / 24.3	C0.2 / 23.3	C0.0 / 23.6	C0.1 / 24.6
F0.1 / 24.3	F0.2 / 23.3	C0.5 / 24.3	C0.6 / 25.3
F0.1 / 24.3	F0.2 / 23.3	C0.1 / 23.7	C0.2 / 24.7
C0.2 / 24.7	C0.1 / 23.7	C0.6 / 24.5	C0.6 / 25.5
C0.9 / 25.8	C0.8 / 24.8	C0.4 / 24.2	C0.6 / 25.2
C1.8 / 26.8	C1.5 / 25.8	Not set ℄ at sidewalk — / 24	—
F0.1 / 24.2	F0.3 / 23.2	C0.3 / 24.0	C0.6 / 25.0
F0.8 / 23.3	F0.9 / 22.3	F0.9 / 22.3	F0.8 / 23.3
F1.3 / 22.4	F1.5 / 21.4	F1.2 / 21.8	F1.0 / 22.8

		1212.12			
70			7.09 0.71	1211.71	
	7.31	1218.80	0.63	1211.99	
71			5.02	1213.78	
72			2.94	1215.86	
73			0.87	1217.93	
	5.40	1223.62	0.58	1218.22	
74			4.06	1219.56	
75			3.33	1220.29	
DM#1	3.84	1223.57	3.84	1219.78	1219.73
76			2.65	1220.92	
	7.22	1228.64	2.15	1221.42	
77			6.40	1222.24	
78			4.41	1224.23	
79			1.72	1226.92	
	10.25	1237.31	1.58	1227.06	
80			7.01	1230.30	
81			3.86	1233.45	

F0.6 23.6	F0.7 23.6	F1.6 21.2	F1.3 22.2
F0.2 24.9	C0.2 23.9	C0.4 24.2	C0.4 25.2
F0.9 23.3	F0.9 22.3	F0.4 23.0	F0.2 24.0
F1.2 22.5	F1.4 21.5	F0.1 23.5	C0.1 24.5
C0.0 24.6	C0.0 23.6	C0.7 24.6	C0.5 25.6
F1.2 22.8	F1.2 21.8	F1.4 21.5	F1.3 22.5
F2.4 21.0	F2.4 20.0	F2.6 19.7	F2.5 20.7
F2.3 21.2	F2.3 20.2	F2.1 20.5	F2.1 21.5
F1.2 22.5	F1.4 21.5	F1.5 21.4	F1.3 22.4
C0.3 25.0	C0.3 24.0	C0.3 24.0	C0.6 25.0
C1.3 26.5	C1.3 25.5	C2.1 26.7	C2.3 27.7
C0.4 25.2	C0.4 24.2	C0.4 24.2	C0.5 25.2

		1237.31						
82			1.81	1235.50		F1.6 / 22.2	F1.6 / 21.2	F1.9 / 20.8	F1,8 / 21.8
83			0.31	1237.00		F0.3 / 23.9	F0.5 / 22.9	F1.6 / 21.2	F1.6 / 22.2
	5.23	1241.92	0.62	1236.69					
84			4.11	1237.81		C0.3 / 25.0	C0.3 / 24.0	C 1.7 / 26.1	C 1.9 / 27.1
~~BM#8~~					~~1237.28~~				
85			4.67	1233.25		F1.8 / 22.2	F1.6 / 21.2	C0.6 / 24.5	C0.8 / 25.5
86			5.44	1236.48		F1.8 / 21.6	F2.0 / 20.6	F0.2 / 23.3	C 0.0 / 24.3
87			5.25	1236.67		F2.2 / 21.2	F2.2 / 20.3	F2.0 / 20.6	F1.8 / 21.6
	5.09	1241.28	5.73	1236.19					
88			3.95	1237.33		F3.4 / 21.5	F3.2 / 20.5	F3.1 / 20.3	F3.0 / 21.3
	4.74	1240.93	5.09	1236.19					
BM#8	3.61	1240.89	3.61	1237.32	1237.28				
	4.86	1241.90	3.85	1237.04					
89			3.90	1238.00		F3.5 / 22.2	F3.6 / 21.3	F3.7 / 21.5	F3.7 / 22.5
90			3.23	1238.67		F2.1 / 21.3	F2.2 / 20.3	F2.6 / 19.9	F2.1 / 20.9
91			2.57	1239.33		F0.4 / 24.2	F0.3 / 23.2	C0.0 / 23.6	C0.3 / 24.6
	3.82	1244.70	1.02	1240.88					
92			5.05	1239.65		C0.6 / 25.2	0.04 / 24.2	C2.6 / 27.5	C 3.0 / 28.5
93			5.45	1239.25		C1.0 / 26.1	C 1.0 / 25.1	C2.3 / 27.0	C2.4 / 28.0

		1244.70			
94			6.20	1238.50	
95			6.78	1237.72	
	8.03	1245.95	6.78	1237.92	
96			7.48	1238.47	
97			5.61	1240.34	
98			2.74	1243.19	
13M#9	5.03	1249.36	1.82	1244.33	
	3.27	1249.28	3.27	1246.09	1246.01
99			3.99	1245.29	
100			3.23	1246.05	
101			3.38	1245.90	
102			3.68	1245.60	
	4.41	1248.67	5.02	1244.26	
103			3.37	1245.30	
T.P. Hubat Lot 6 of 103			5.08	1243.59	
104				1244.78	
105				1243.80	

F2.0 / 21.8	F1.9 / 20.8	F0.4 / 23.0	F0.2 / 24.0
F2.3 / 21.5	F2.1 / 20.5	F1.7 / 21.1	F1.7 / 22.1
F0.6 / 22.4	F0.8 / 22.4	F0.8 / 22.4	F0.7 / 23.4
C1.6 / 27.0	C1.6 / 26.0	C1.5 / 25.8	C1.6 / 26.8
C1.8 / 26.8	C1.5 / 25.8	C1.4 / 25.7	C1.5 / 26.7
C0.1 / 24.6	C0.0 / 23.6	C0.4 / 24.2	C0.6 / 25.2
F1.4 / 22.1	F1.7 / 21.1	F1.9 / 20.8	F1.8 / 21.8
F0.9 / 23.4	F0.8 / 22.4	F0.8 / 22.4	F0.5 / 23.4
F1.5 / 22.4	F1.5 / 21.4	F1.2 / 21.8	F1.0 / 22.8
F1.7 / 21.6	F2.0 / 20.6	F1.4 / 21.5	F1.1 / 22.5
—	21.5	23	—
—	21	24	—

7/10/29 Richey Canfield Grain

BM #10	755	1248.41			1240.86
104			3.63	1244.78	
105			4.61	1243.80	
106			5.81	1242.60	
107			6.71	1241.70	
108			7.02	1241.39	
	2.93	1243.22	8.12	1240.29	
109			2.15	1241.07	
110			2.46	1240.76	
111			2.78	1240.44	
112			3.09	1240.13	
	7.42	1246.60	4.04	1239.18	
113			6.64	1239.96	
114			5.72	1240.88	
BM #11	3.05	1246.57	3.05	1242.55	1240.52
115			3.52	1243.05	

F1.0 / 22.9	F1.2 / 21.8		C0.6 / 24.5	C0.6 / 25.5
F1.3 / 22.7	F1.3 / 21.7		C1.0 / 25.1	C1.3 / 26.1
F2.3 / 21.3	F2.2 / 20.3		F0.5 / 22.9	F0.2 / 23.9
F1.6 / 24.5	F1.4 / 21.5	← Special 2' Ditch →	C0.2 / 23.9	C0.9 / 26.9
F2.2 / 22.6	F2.0 / 20.6	"	F0.6 / 22.7	F0.4 / 25.7
F1.8 / 23.8	F1.9 / 20.8	"	F0.5 / 22.9	C0.1 / 25.9
F1.4 / 24.5	F1.4 / 21.5	← " →	F0.3 / 23.2	C0.1 / 26.2
F3.3 / 22.1	F3.5 / 21.1	Special 2' Ditch →	F2.0 / 20.6	F1.8 / 23.6
F2.6 / 20.9	F2.5 / 19.9		F2.6 / 19.7	F2.4 / 20.7
F1.6 / 21.9	F1.8 / 20.9		F1.3 / 21.7	F1.2 / 22.2
C0.5 / 25.0	C0.3 / 24.0		C0.2 / 23.9	C0.5 / 24.9
C1.7 / 26.8	C1.5 / 25.8		C0.1 / 23.7	C0.3 / 24.7

		1246.57			
	11.76	1257.91	0.42	1246.15	
116			11.61	1246.30	
117			8.21	1249.90	
118			4.81	1253.10	
	6.78	1263.20	1.49	1256.42	
119			7.09	1256.11	
120			4.77	1258.43	
121			2.84	1260.36	
	8.71	1269.36	2.55	1260.65	
122			7.07	1262.29	
123			5.14	1264.22	
T.P. Lt of ℄	6.60	1270.83	5.13	1264.23	
124			4.68	1266.15	
New B.M.			5.75		1265.08
125			2.75	1268.08	
BM #12	Gone				1268.27
126			1.26	1269.57	
	5.12	1274.28	1.67	1269.16	
127			4.08	1270.20	

C1.6 / 26.8	C1.5 / 25.8	C1.3 / 25.5	C1.5 / 26.5
C1.8 / 27.1	C1.7 / 26.1	C1.4 / 25.7	C1.6 / 26.7
C2.1 / 27.6	C2.0 / 26.6	C1.6 / 26.0	C1.7 / 27.0
C1.4 / 26.5	C1.3 / 25.5	C1.2 / 25.4	C1.3 / 26.4
F0.2 / 24.2	F0.2 / 23.2	C0.0 / 23.1	C0.1 / 24.6
F1.0 / 22.2	F1.3 / 21.7	F0.5 / 22.9	F0.4 / 23.9
F0.5 / 23.4	F0.8 / 22.4	C0.1 / 23.7	C0.4 / 24.7
C0.0 / 24.6	C0.0 / 23.6	C0.9 / 24.9	C1.0 / 25.9
C0.9 / 25.5	C0.6 / 24.5	F0.1 / 23.5	C0.0 / 24.5

Spike in root of 12" Beech 35' Lt of ℄ 123+15

C0.2 / 24.7	C0.1 / 23.7	F0.7 / 22.6	F0.9 / 23.6
F0.9 / 22.1	F1.0 / 22.1	F1.3 / 21.7	F1.5 / 22.7
F0.8 / 23.4	F0.8 / 22.4	F1.2 / 21.8	F1.4 / 22.8

		1274.28		
128			3.88	1270.40
129			3.68	1270.60
130			3.48	1270.80
131			3.28	1271.00
	5.72	1275.86	4.14	1270.14
132			4.66	1271.20
133			4.41	1271.45
134			3.81	1272.05
135			2.86	1273.00
	7.37	1280.29	2.94	1272.92
136			6.29	1274.00
137			5.29	1275.00
138			4.29	1276.00
139			3.29	1277.00

New BM

F0.8 / 23.1	F1.0 / 22.1	F1.2 / 21.8	F1.3 / 22.8
F0.1 / 24.5	F0.1 / 23.1	F0.6 / 22.7	F0.5 / 23.7
F0.9 / 23.0	F1.1 / 22.0	F1.0 / 22.1	F1.0 / 23.1
F1.1 / 22.7	F1.3 / 21.7	F1.1 / 22.0	F1.0 / 23.0
F1.2 / 22.7	F1.3 / 21.7	F1.0 / 22.1	F0.9 / 23.1
F1.4 / 22.4	F1.5 / 21.4	F1.3 / 21.7	F1.6 / 22.7
F1.0 / 23.0	F1.1 / 22.0	F1.0 / 22.1	F0.8 / 23.1
F0.5 / 23.6	F0.7 / 22.6	F0.4 / 22.0	F0.5 / 24.0
F0.2 / 24.0	F0.4 / 23.0	C0.0 / 22.6	C0.1 / 24.6
C0.0 / 24.2	F0.3 / 23.2	C0.3 / 24.0	F0.2 / 25.0
F0.1 / 24.2	F0.3 / 23.2	C0.3 / 24.0	C0.5 / 25.0
F0.9 / 23.0	F1.1 / 22.0	F0.7 / 22.6	F0.5 / 23.6

		1280.29							
140			2.41	1277.88		F0.7 / 23.3	F0.9 / 22.3	F0.7 / 22.6	F0.6 / 23.6
BM#13	2.96	1281.09	2.05	1278.24	1278.13				
141			3.21	1277.88		F0.9 / 23.1	F1.0 / 22.1	F0.5 / 22.9	F0.3 / 23.9
142			4.09	1277.00		F0.8 / 23.3	F0.9 / 22.3	C0.1 / 23.7	C0.2 / 24.7
143			5.09	1276.00		F0.3 / 24.0	F0.4 / 23.0	E0.2 / 23.3	F0.1 / 24.3
New B.M.			4.00	1277.09	1277.09	Spike in NE ¼ of barn 30' Lt of Sta 142+60			
144				1275.00		—	20	23	—
145				1274.63		—	22	24.5	—
146				1274.25		—	22	24	—
147				1273.88		—	22	22.5	—

7/17 Richey Canfield Grau

BM.	2.11	1279.20			1277.09
144			4.20	1275.00	
145			4.57	1274.63	
146			4.95	1274.25	
	3.44	1277.09	5.55	1273.65	
147			3.21	1273.88	
148			3.59	1273.50	
BM #14	4.41	1277.11	4.41	1272.68	1272.70
149			3.98	1273.13	
150			4.36	1272.75	
151			4.73	1272.38	
	2.80	1274.06	5.85	1271.26	
152			2.25	1271.81	
153			3.17	1270.89	
154			4.28	1269.78	
155			5.39	1268.67	

F2.1 / 21.3	F2.2 / 20.3	F1.1 / 22.0	F1.1 / 23.0
F0.4 / 23.9	F0.5 / 22.9	C1.1 / 25.2	C1.2 / 26.2
F0.6 / 23.4	F0.8 / 22.4	C0.8 / 24.8	C0.8 / 25.8
F0.9 / 23.1	F1.0 / 22.1	F0.1 / 23.5	C0.1 / 24.5
F1.3 / 22.7	F1.5 / 21.4	F1.1 / 22.0	F1.0 / 23.0
F1.6 / 22.1	F1.7 / 21.1	F0.6 / 22.7	F0.4 / 23.7
F1.2 / 22.5	F1.4 / 21.5	F0.5 / 22.9	F0.3 / 23.9
F0.2 / 23.2	F0.9 / 22.3	C0.3 / 24.0	C0.5 / 25.0
F1.4 / 22.5	F1.4 / 21.5	F0.2 / 23.3	F0.1 / 24.3
F1.1 / 23.0	F1.1 / 22.0	C0.3 / 24.0	C0.5 / 25.0
F1.2 / 22.7	F1.3 / 21.7	F1.0 / 22.7	F0.7 / 23.1
F1.3 / 22.7	F1.3 / 21.7	F0.9 / 22.3	F0.9 / 23.3

		1274.06		
156			6.37	1267.69
	6.83	1273.22	7.67	1266.39
157			5.62	1267.60
158			4.81	1268.41
BM #15	4.79	1273.18	4.79	1268.43 / 1268.39
159			3.83	1269.35
160			2.89	1270.29
161			1.95	1271.23
	7.30	1276.83	3.65	1269.53
162			4.66	1272.17
163			3.72	1273.11
164			2.78	1274.05
165			2.38	1274.45
New BM 162+85			0.26	1276.57
166			3.11	1273.72
	4.38	1278.03	3.18	1273.65
167			5.15	1272.88

F2.1 / 21.8	F1.9 / 20.8	F1.7 / 21.1	F1.5 / 22.1
F1.3 / 22.7	F1.3 / 21.7	F0.8 / 22.4	F0.6 / 23.4
F0.4 / 23.9	F0.5 / 22.9	C1.0 / 25.1	C1.3 / 24.1
F0.4 / 23.6	F0.7 / 22.6	C0.4 / 24.2	C0.7 / 25.2
F1.1 / 22.8	F1.2 / 21.8	C0.2 / 23.9	C0.5 / 24.9
F1.7 / 22.1	F1.7 / 21.1	F0.4 / 23.0	F0.3 / 24.0
F2.1 / 21.2	F2.3 / 20.2	F1.3 / 21.7	F0.9 / 22.7
F1.8 / 21.6	F2.0 / 20.6	F1.3 / 21.7	F1.0 / 22.7
F0.9 / 23.3	F0.9 / 22.3	C0.3 / 24.0	C0.4 / 25.0
F0.1 / 24.2	F0.2 / 23.3	C0.9 / 24.9	C0.9 / 25.9
Spike in top of 18" Stump 35' Rt of ℄			
C0.1 / 24.3	F0.2 / 23.3	C1.0 / 25.1	C1.0 / 26.1
F1.3 / 22.4	F1.5 / 21.4	F0.2 / 23.3	F0.1 / 24.3

		1278.03		
168			5.13	1272.90
169			4.23	1273.80
	11.46	1287.93	1.56	1276.47
170			12.34	1275.59
171			9.68	1278.25
172			6.67	1281.26
BM #16	4.41	1287.93	4.41	1283.52 / 1283.52
173			4.32	1283.61
174			2.71	1285.22
	4.57	1289.77	2.73	1285.20
175			3.68	1286.09
176			3.47	1286.30
177			3.40	1286.37
178			3.71	1286.06
179			4.40	1285.37
	3.54	1287.52	5.79	1283.98

F2.7 / 20.9	F2.5 / 19.9	F1.5 / 21.4	F0.9 / 22.4
F2.0 / 21.5	F2.1 / 20.5	F1.2 / 21.8	F1.0 / 22.8
C2.2 / 27.4	C1.9 / 26.4	C0.8 / 24.8	C0.8 / 25.8
C2.6 / 28.2	C2.4 / 27.2	C1.5 / 25.8	C1.4 / 26.8
C1.0 / 25.9	C0.9 / 24.9	C1.2 / 25.4	C1.4 / 26.4
F0.2 / 24.2	F0.3 / 23.2	C0.9 / 24.9	C1.1 / 25.9
F0.9 / 23.0	F1.1 / 22.0	C0.0 / 23.6	C0.2 / 24.6
F2.1 / 21.5	F2.1 / 20.5	C0.3 / 24.0	C0.6 / 25.0
F1.6 / 22.4	F1.5 / 21.4	C0.7 / 24.6	C0.8 / 25.6
F2.1 / 21.5	F2.1 / 20.5	F0.6 / 22.7	F0.3 / 23.7
F1.6 / 22.1	F1.7 / 21.1	C0.1 / 23.7	C0.4 / 24.7
F2.0 / 21.6	F2.0 / 20.6	F0.6 / 22.7	F0.4 / 23.7

	1287.82						
180		2.90	1284.62		F1.4 / 22.5	F1.4 / 21.5	F0.1 / 23.5 F0.1 / 24.5
New BM		3.26		1284.26	Spike in W Root of 24" Elm 25' Rt of ℄ at 180+75		
181		3.65	1283.87		F1.3 / 22.7	F1.3 / 21.7	F1.4 / 23.0 F0.1 / 24.0
182		4.40	1283.12		F0.2 / 24.0	F0.4 / 23.0	F0.1 / 23.5 C0.4 / 24.5
183		4.74	1282.78		F0.8 / 23.3	F0.9 / 22.3	F0.5 / 22.9 F0.3 / 23.9
T.P. Rock Lt of ℄		4.07	1283.45				
184			1282.33		—	23	23.5 —
185			1284.77		—	22	20.5 —
186			1286.62		—	23	24 —
187			1288.47		—	23	24 —
188			1290.32		—	25.5	23 —
189			1292.16		—	22.5	23 —
190			1293.55		—	22	24.5 —
B.M. #17				1294.88			
191			1294.06		—	22	23.5 —

		P/O	Richey Parks Hoffman		
New BM	3.80	1288.06			1289.26
184			4.73	1283.33	
185			3.29	1284.77	
	10.24	1295.56	2.74	1285.32	
186			8.94	1286.62	
187			7.09	1288.47	
188			5.24	1290.32	
189			3.40	1292.16	
	5.75	1297.95	3.36	1292.20	
190			4.40	1293.55	
BM #17	3.26	1298.14	3.26	1294.69	1294.88
191			4.08	1294.06	
192			4.02	1294.12	
193			3.96	1294.18	
194			3.90	1294.24	
195			3.84	1294.30	
	4.76	1298.46	4.44	1293.70	

F0.4 / 23.9	F0.5 / 22.9			C0.1 / 23.7	C0.3 / 24.7
F0.5 / 23.6	F0.7 / 22.6			C0.1 / 23.7	C0.1 / 24.7
C0.2 / 24.6	C0.0 / 23.6			C0.5 / 24.3	C0.5 / 25.3
C0.5 / 25.5	C0.6 / 24.5			C1.2 / 25.4	C1.4 / 26.4
F0.6 / 23.6	F0.7 / 22.6			C0.2 / 23.9	C0.3 / 24.9
F0.2 / 24.3	F0.2 / 23.3			C0.1 / 23.7	C0.1 / 24.7
F0.3 / 24.0	F0.4 / 23.0			C0.5 / 24.3	C0.7 / 25.3
F0.4 / 23.7	F0.6 / 22.7			C0.1 / 23.7	C0.2 / 24.7
F1.3 / 22.4	F1.5 / 21.4			F0.7 / 22.6	F0.6 / 23.6
F1.9 / 21.6	F2.0 / 20.6			F1.0 / 22.1	F1.0 / 23.1
F2.0 / 21.8	F1.9 / 20.8			F1.0 / 22.1	F0.9 / 23.1
F1.7 / 21.9	F1.8 / 20.9			F0.6 / 22.7	F0.5 / 23.7

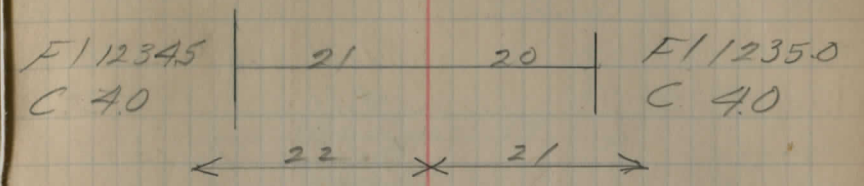
~~195~~

	129.46						
196		4.10	129.36	F1.7 / 21.9	F1.8 / 20.9	F0.7 / 22.6	F0.4 / 23.6
197		4.04	129.42	F1.6 / 22.1	F1.7 / 21.1	F0.1 / 23.5	C0.1 / 24.5
198		4.50	129.96	F1.7 / 22.2	F1.6 / 21.2	F0.4 / 23.0	F0.4 / 24.0
199		6.02	129.44	C0.2 / 24.3	F0.2 / 23.3	C0.9 / 24.9	C0.9 / 25.9
200		8.58	128.88	C1.0 / 26.1	C1.0 / 25.1	C1.1 / 25.2	C1.2 / 26.2
BM#18		9.56	128.90				
			128.74				
201			128.79	—	23	24	—
202			128.71	—	23.5	24.5	—
203			128.62	—	24	25	—
204			127.42	—	23.5	25.5	—
205			127.38	—	24.5	26.5	—
206			126.50	—	25	27	—
207			126.38	—	24.5	26.5	—

7/14/29

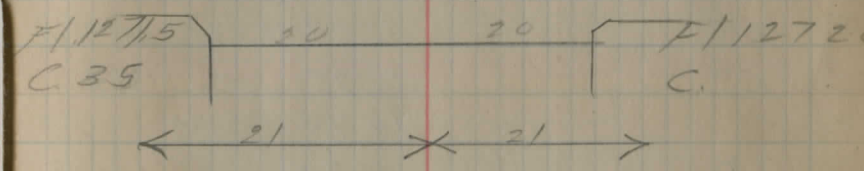
BM#11	0.11	1243.63			1243.52
Flow R			8.51	1235.12	1235.0
Stake R			4.51		C 4.0
Flow L			9.25	1234.38	1234.5
Stake L			5.25		C 4.0

No 15 Sta 111+46



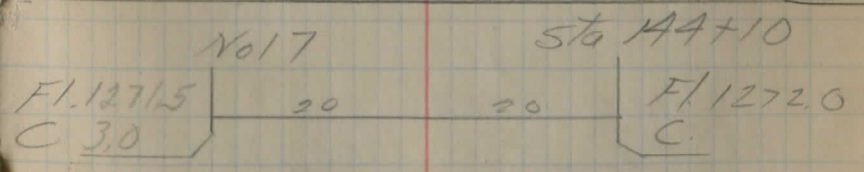
BM#12	5.71	1278.41			1272.70
Flow E			6.29	1272.12	1272.0
Stake E			2.79		C 3.5
Flow W			7.03	1271.38	1271.5
Stake W			3.53		C 3.5

No 16 Sta 143+81



BM#12	5.71	1278.41			1272.70
Flow E			6.29	1272.12	1272.0
Stake E			1.29		C 5.0
Flow W			7.03	1271.38	1271.5
Stake W			4.03		C 3.0

No 17 Sta 144+10



7/23/29

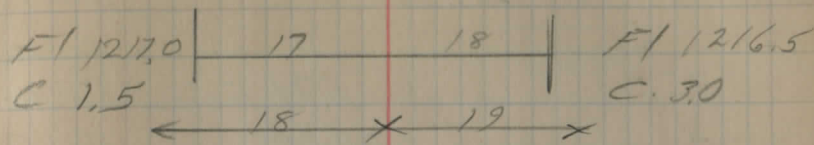
BM #7	4.36	1224.09			1219.73
Flow E			7.71	1216.38	1216.5
Stake E			4.71		C 3.0
Flow W			6.97	1217.12	1217.0
Stake W			5.97		C 1.5

7/24/29

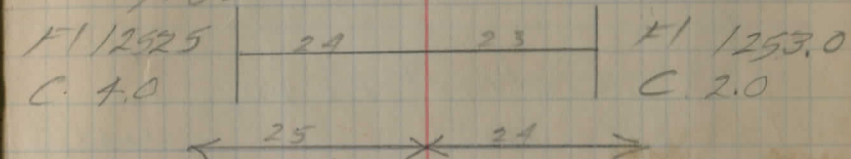
BM #19	0.77	1265.18			1264.41
Flow R			12.08	1253.10	1253.0
Stake R			10.88		C 2.0
Flow L			12.78	1252.40	1252.5
Stake L			8.78		C 4.0

BM #16	1.40	1284.92			1283.52
	2.21	1278.70	8.43	1276.49	
Flow R			9.08	1269.62	1269.5
Stake R			5.58		C 3.5
Flow L			9.82	1268.88	1269.0
Stake L			7.32		C 2.5

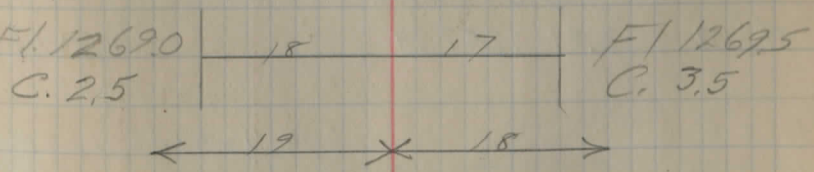
Extra 12" VSP. Sta 76+25



No 22 Sta 208+93



No 19 Sta 168+07



7/26/29

BM #15	3.00	1271.39			1268.39
Flow R			6.74	1264.65	1264.5
Stake R			5.24		C 1.5
Flow L			7.54	1263.85	1264.0
Stake L			5.54		C 2.0

Culvert No 20

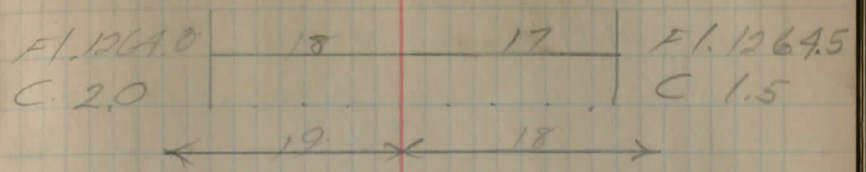
BM	3.07	1287.33			1284.26
Flow R			6.68	1280.65	1280.50
Stake R			2.18		C 4.5
Flow L			7.98	1279.85	1280.00
Stake L			4.48		C 3.0

Culvert No 21

BM #17	2.81	1297.69			1294.88
Flow R			6.04	1291.65	1291.5
Stake R			3.04		C 3.0
Flow L			6.84	1290.85	1291.0
Stake L			4.34		C 2.5

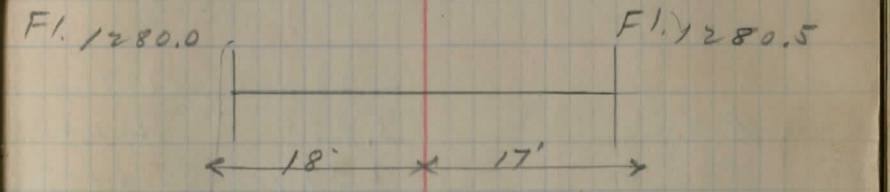
Culvert No 18

℄ Sta 156+33



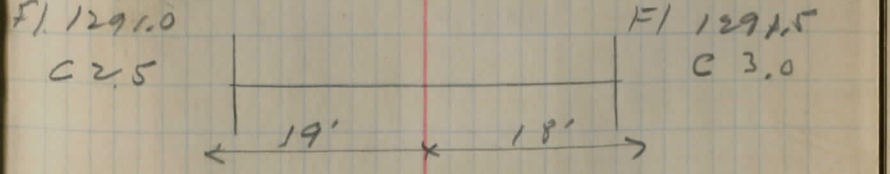
Culvert No 19

℄ Sta 182+74



Culvert No 20

℄ Sta 193+22



Culvert No 23

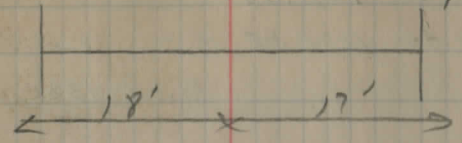
BM	3.44	1276.95		1273.51
	4.41	1271.47	9.89	1267.06
Flow R			6.32	1265.15 / 1265.0
Stake R			2.82	C 3.5
Flow L			7.12	1264.35 / 1264.5
Stake L			4.62	C 2.5

℄ Sta 217+38

Fl. 1264.5

Fl. 1265.0

C 3.5



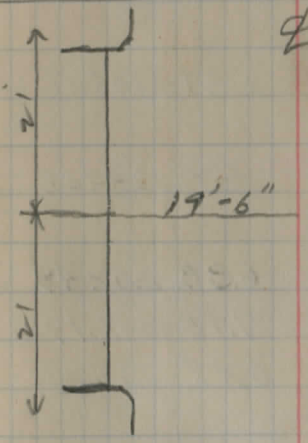
Culvert No 24

BM	3.44	1276.95		1273.51
Flow N			6.33	1270.62 / 1270.5
Stake N			3.83	C 2.5
Flow S			7.57	1269.38 / 1269.5
Stake S			5.07	C 2.5

℄ Sta 220+54

Fl. N 1270.5

C 2.5



Fl. S 1269.5

C 2.5

BM 22	0.43	1271.03			1270.60
	0.44	1258.66	12.81	1258.22	
245			8.12	1250.54	
246			10.43	1248.23	
	1.99	1249.37	11.28	1247.38	
247			2.54	1246.83	
248			3.81	1245.56	
249			5.09	1244.28	
250			6.88	1242.49	
	3.94	1246.13	7.18	1242.19	
251			6.47	1239.66	
252			10.20	1236.33	
	0.24	1236.37	10.00	1236.13	
253			2.49	1233.88	
254				1233.07	
BM 23	2.85	1236.39	2.85	1233.52	1233.54

240+50 Maple 30' Lt ℄

C 1.2 / 25.9	C 0.9 / 24.9	C 4.9 / 29.1	C 5.2 / 30.1
F 0.1 / 24.5	F 0.1 / 23.5	C 2.3 / 27.0	C 2.8 / 28.0
F 1.9 / 21.9	F 1.8 / 20.9	F 1.0 / 22.1	F 0.8 / 23.1
F 2.1 / 21.6	F 2.0 / 20.6	F 2.1 / 20.5	F 2.0 / 21.5
F 1.6 / 22.5	F 1.4 / 21.5	F 1.5 / 21.7	F 1.4 / 22.4
F 0.3 / 24.0	F 0.4 / 23.0	C 0.3 / 24.0	C 0.4 / 25.0
C 1.1 / 26.4	C 1.2 / 25.4	C 2.6 / 27.5	C 2.6 / 28.5
C 1.6 / 26.5	C 1.3 / 25.5	C 3.1 / 28.2	C 3.5 / 29.2
F 1.2 / 22.8	F 1.2 / 21.8	F 0.9 / 22.2	F 0.8 / 23.3
	19.5	20.	

254+00 "X" SE cor E Hdwall

		1236.39		
255			3.26	1233.13
256			3.19	1233.20
257			3.12	1233.27
	5.58	1237.94	4.03	1232.36
258			4.61	1233.33
259			4.54	1233.40
260			4.47	1233.47
	4.72	1237.09	5.57	1232.37
261			3.72	1233.37
262			3.98	1233.11
263			4.24	1232.85
	4.66	1235.61	6.14	1230.95
264			3.02	1232.59
265			3.28	1232.33
266			3.54	1232.07
BM 24			3.05	1232.56 1232.51

Special Ditch Lt.		4' Ditch Rt
F2.4 / 28.2	27.2	F0.8 / 26.4 — F0.6 / 27.4
F1.3 / 30.8	29.8	F0.1 / 27.5 — C0.0 / 28.5
F1.0 / 29.8	28.8	F1.0 / 26.1 — F0.9 / 27.1
F0.8 / 29.8	28.8	F0.3 / 27.2 — C0.0 / 28.2
F1.2 / 31.0	30.0	F0.8 / 26.4 — F0.5 / 27.4
F1.1 / 31.0	30.0	F0.8 / 26.4 — F0.6 / 27.4
F0.8 / 31.0	30.0	F0.8 / 26.4 — F0.7 / 27.4
F1.6 / 29.0	28.0	F1.9 / 24.8 — F1.7 / 25.8
F1.9 / 27.5	26.5	F1.9 / 24.8 — F1.7 / 25.8
F0.7 / 27.7	26.7	F1.9 / 24.8 — F1.7 / 25.8
F2.3 / 24.5	23.5	F2.1 / 24.5 — F2.0 / 25.5
F1.2 / 26.5	25.5	F0.7 / 26.6 — F0.4 / 27.6

267+30 Maple 25' Rt ℄

Culvert No 30

BM	2.65	1235.16			1232.51
	3.43	1234.33	4.26	1230.90	
Flow R			6.18	1229.15	1225.0
Stake R			3.68		C 2.5
Flow L			6.98	1227.35	1227.5
Stake L			5.48		C 1.5

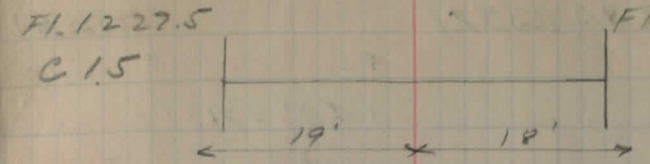
Culvert No. 31

T.P.	3.80	1234.46			1230.66
Flow R			4.81	1229.65	1229.5
Stake R			1.81		C 3.0
Flow L			5.61	1228.85	1229.0
Stake L			3.11		C 2.5

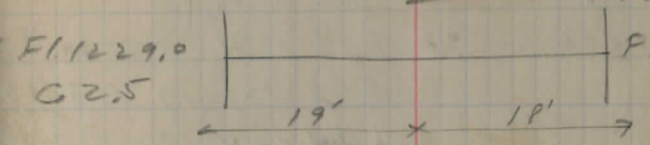
Culvert No 32

BM	5.36	1237.50			1232.14
Flow R			5.38	1232.12	1232.0
Stake R			2.88		C 2.5
Flow L			6.62	1230.88	1231.0
Stake L			3.12		C 3.5

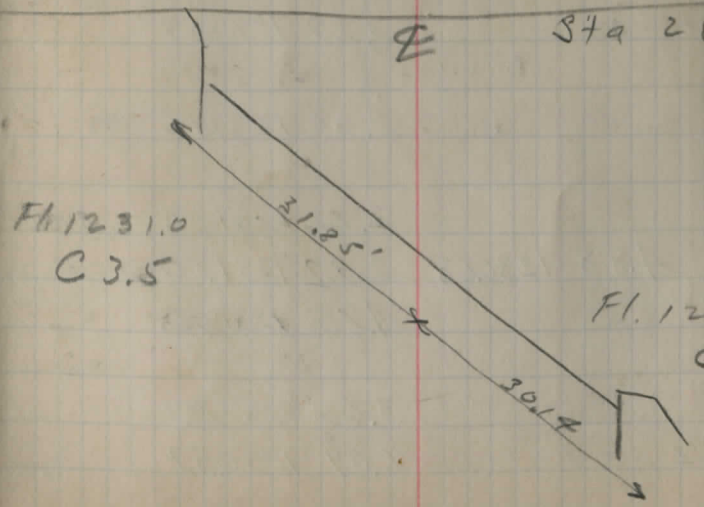
℄ Sta 272+50



℄ Sta 276+66



℄ Sta 284+81



		8/22/29		Richey Park St Canfield	
BM #24	2.70	1235.21			1232.51
267			3.40	1231.81	
268			3.67	1231.55	
269			3.92	1231.29	
270			4.18	1231.03	
New BM			0.02	1235.19	1235.19
271			4.44	1230.77	
	5.05	1234.12	6.14	1229.07	
272			3.46	1230.66	
273			3.29	1230.83	
274			2.96	1231.16	
275			2.62	1231.50	
	4.88	1236.68	2.32	1231.80	
276			4.75	1231.93	
277			3.69	1232.99	
TP Slope L			6.09	1230.59	

F1.0 / 27.8	F1.2 / 26.8	5' Ditch	F0.8 / 27.4	F0.7 / 28.4
F0.6 / 28.6	F0.7 / 27.6	"	C0.5 / 29.3	C0.6 / 30.3
F1.2 / 27.5	F1.4 / 26.5	"	C0.3 / 29.0	C0.5 / 30.0
F2.0 / 26.8	F1.9 / 25.8	"	F1.3 / 26.7	F1.1 / 27.7
2 spikes in root 24" Ash 300' Rt ℄ Sta 270+50				
F1.7 / 26.9	F1.8 / 25.9	"	F1.5 / 26.4	F1.3 / 27.4
F1.6 / 27.1	F1.7 / 26.1	"	F1.5 / 26.4	F1.5 / 27.4
F1.8 / 26.5	F2.1 / 25.5	"	F1.6 / 26.2	F1.6 / 27.2
F0.6 / 28.6	F0.7 / 27.6	"	C0.0 / 28.6	C0.0 / 29.6
C0.3 / 29.9	C0.2 / 28.9	"	C0.4 / 29.2	C0.5 / 30.2
F1.8 / 26.8	F1.9 / 25.8	"	F1.2 / 26.8	F1.0 / 27.8
F2.4 / 21.0	F2.4 / 20.0		F2.0 / 20.6	F1.9 / 27.6

		8/23/29		Rainey Road Canfield	
BM #22	0.76	127.36			1270.00
	8.89	126.271	12.54	258.82	
241			8.83	1253.58	
			4.44	1258.27	
	10.96	127.98	0.19	126.252	
242			9.41	1263.57	
241			4.46	1268.52	
	10.77	128.137	2.37	127061	127060
240			8.87	1272.50	
239			5.37	1276.00	
	9.38	1286.92	3.83	1277.54	
238			7.42	1279.50	
237			4.80	1282.12	
236			3.92	1283.00	
235			3.92	1283.00	
New BM	1.98	1286.47	2.43	1284.49	
234				1283.14	
233				1283.58	
BM #21			2.37	1284.10	1284.10

E0.8 / 23.2	22.2	Special	27.3	C2.9 / 28.3
C1.0 / 24.5	23.5	Special	25.7	E1.1 / 26.7
C1.8 / 26.6	25.6	Special	30.0	C4.0 / 31.0
F1.6 / 22.4	F1.5 / 21.4		C1.4 / 27.7	C1.7 / 26.7
E0.3 / 24.0	E0.4 / 23.0		E1.4 / 21.5	E1.3 / 22.5
C0.4 / 25.0	C0.3 / 24.0		C1.3 / 25.5	C1.6 / 26.5
C0.1 / 24.6	C0.0 / 23.6		C1.3 / 25.5	C1.5 / 26.5
E1.2 / 22.8	F1.2 / 21.8		C0.1 / 23.7	C0.3 / 24.7
E0.8 / 23.4	E0.8 / 22.4		C0.4 / 24.2	C0.7 / 25.2
E0.5 / 23.6	E0.7 / 22.6		C1.1 / 25.2	C1.3 / 26.2

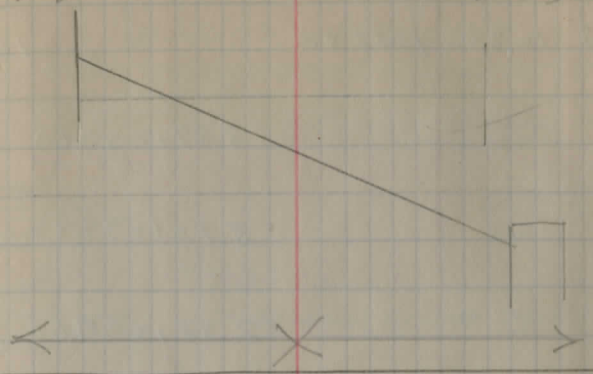
2 Spikes in root 15" Maple 36' Rt & Sta 235+00

— 20 — 22 —

— 19 — 21.5 —

BM #22	076				

NO 28 243+78



BM #21	2.37	1286.47			1284.10
Flow R			6.82	1279.65	1279.5
stake R			332	C35	
Flow L			7.62	1278.85	1279.0
stake L			462	C30	

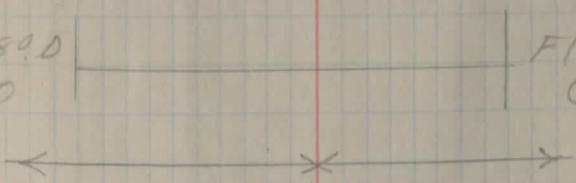
NO 27 233+48

Fl. 1279.0 C. 3.0 — Fl 1279.5 C 3.5

BM #21	2.37	1286.47			1284.10
Flow R			5.82	1280.65	1280.5
stake R			282		C3.0
Flow L			6.62	1279.85	1280.0
stake L			362		C30

NO 26 231+67

Fl. 1280.0 C 3.0 — Fl 1280.5 C 3.0



8/26 Richey Parks Rand Canfield

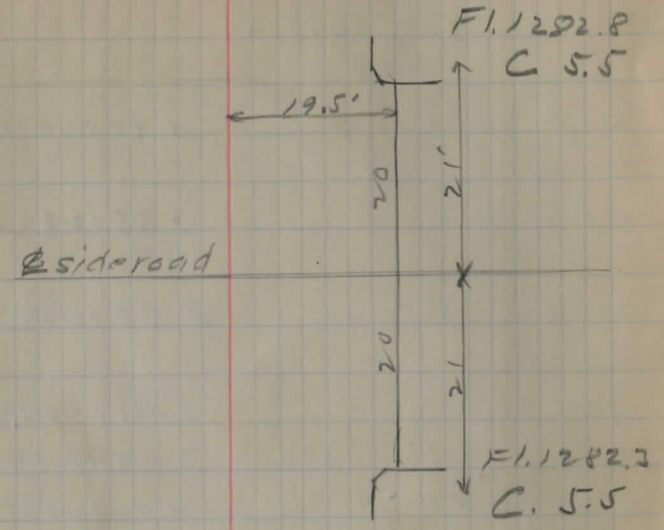
BM#25	10.36	1242.50			1232.14
285			8.87	1233.63	
284			5.13	1237.37	
283			2.88	1239.62	
282			2.50	1240.00	
	0.22	1240.64	2.08	1240.42	
281			1.08	1239.56	
280			2.41	1238.23	
279			4.19	1236.45	
278			5.97	1234.67	

—	21.5	22.5	—
C 1.2 / 26.2	C 1.1 / 25.2	C 0.7 / 24.6	C 1.1 / 25.6
F 0.9 / 23.0	F 1.1 / 22.0	Summit Sec → F 0.4 / 15.2	C 0.1 / 16.2
F 0.9 / 23.1	F 1.0 / 22.1	F 0.9 / 23.3	F 0.7 / 23.3
F 1.2 / 22.7	F 1.3 / 21.7	F 0.5 / 22.9	F 0.3 / 23.9
F 0.7 / 23.3	F 0.9 / 23.3	F 0.9 / 22.3	F 0.4 / 23.3
F 0.3 / 24.0	F 0.4 / 23.0	F 1.1 / 22.0	F 0.9 / 23.0
F 1.2 / 22.8	F 1.2 / 21.8	F 1.6 / 21.2	F 1.3 / 22.2

Culvert No

BM 21	5.85	1289.95		1284.10
Flow N			7.0 3	1282.92 1282.8
Stake N			1.53	C 5.5
Flow S			7.77	1282.18 1282.3
Stake S			2.27	C 5.5

℄ Sta



BM #21	3.03	1287.13		1284.10
234			3.99	1283.14
233			3.55	1283.58
232			2.98	1284.15
231			2.41	1284.72
	6.01	1290.11	3.03	1284.10
230			4.82	1285.29
229			4.25	1285.86
228			3.68	1286.43
	3.23	1288.75	4.59	1285.52
227			2.45	1286.30
226			3.97	1284.78
225			6.18	1282.57
224			8.39	1280.36
	2.21	1280.65	10.41	1278.34
223			2.50	1278.15

F1.9 / 21.6	F2.0 / 20.6	F0.8 / 22.4	F0.5 / 23.4
F2.2 / 20.7	F2.6 / 19.7	F1.3 / 21.7	F1.0 / 22.7
F2.6 / 20.7	F2.6 / 19.7	F1.2 / 21.8	F1.1 / 22.8
F1.7 / 21.9	F1.8 / 20.9	F0.8 / 22.4	F0.6 / 23.4
F1.5 / 22.1	F1.7 / 21.1	F0.2 / 23.3	F0.1 / 24.3
F2.0 / 21.5	F2.1 / 20.5	C0.5 / 24.3	C0.7 / 25.3
F1.9 / 21.6	F2.0 / 20.6	C0.6 / 24.2	C0.8 / 25.2
F0.6 / 23.9	F0.5 / 22.9	I=0.8 / 22.4	C0.1 / 23.4
F0.3 / 24.2	F0.3 / 23.2	C1.4 / 25.7	C1.6 / 26.7
F2.0 / 21.8	F1.9 / 20.8	C1.1 / 25.2	C1.3 / 26.2
F2.0 / 21.8	F1.9 / 20.8	F1.2 / 21.8	F1.0 / 22.8
F1.2 / 22.8	F1.2 / 21.8	F0.6 / 22.7	F0.4 / 23.7

	1280.65			
222		4.71	1275.94	
221		6.92	1273.73	
BM #20		7.15	1273.50	1273.51
220			1271.52	
219			1269.31	
218			1267.73	
217			1267.40	
216			1268.32	

F 0.3 / 24.3	F 0.3 / 22.3	C 1.6 / 26.0	C 1.9 / 27.0
F 0.4 / 23.6	F 0.7 / 22.6	F 0.6 / 22.7	F 0.2 / 23.7
—	21.5	20	—
—	20.5	22	—
—	20	22	—
—	20	22	—
—	20	22.5	—

5/27

BM#20	0.89	127440			1273.51
220			2.88	1271.52	
219			5.09	1269.31	
218			6.67	1267.73	
217			7.00	1267.40	
	10.17	1275.47	9.10	1265.30	
216			7.15	1268.32	
215			6.19	1269.28	
214			4.25	1271.22	
213			4.38	1271.09	
212			6.46	1269.01	
211			10.02	1265.45	
	0.18	1265.96	9.69	1265.78	
210			3.41	1262.55	
209			4.57	1261.39	

F0.9 / 23.1	F1.0 / 22.1	F2.6 / 19.7	F2.5 / 20.7
F1.6 / 22.4	F1.5 / 21.4	F1.1 / 22.0	F1.0 / 23.0
F2.1 / 21.5	F2.1 / 20.5	F0.7 / 22.6	F0.8 / 23.6
F2.1 / 21.6	F2.0 / 20.6	F1.1 / 22.0	F0.8 / 23.0
F2.0 / 21.8	F1.9 / 20.8	F0.4 / 25.0	F0.3 / 24.0
F0.7 / 23.6	F0.7 / 22.6	C0.7 / 24.6	C1.0 / 25.6
F0.5 / 24.5	F0.1 / 23.5	C2.0 / 26.6	C2.1 / 27.6
C0.3 / 25.0	C0.3 / 24.0	C2.4 / 27.2	C2.6 / 28.2
F0.7 / 23.3	F0.9 / 22.3	C1.4 / 25.7	C1.6 / 26.7
C0.4 / 24.7	C0.1 / 23.7	C3.3 / 28.6	C3.5 / 29.6
F3.8 / 22.1	F3.5 / 21.1	F0.4 / 23.0	F0.2 / 24.0
F7.0 / 27.2	F6.0 / 26.2	F2.8 / 19.7	F2.9 / 20.7

		126.96			
208			3.96	126.00	
	11.14	127.90	1.20	126.76	
207			11.52	126.38	
206			7.40	126.50	
	11.93	127.13	0.70	127.20	
205			13.75	127.38	
204			9.71	127.42	
203			6.51	128.62	
202			3.42	128.71	
	6.88	129.18	2.83	128.30	
201			4.39	128.79	
BM 18			2.54	128.64	128.74

F1.7 / 21.3	F2.2 / 20.3
C1.4 / 25.9	C0.9 / 24.9
C1.4 / 26.7	C1.4 / 25.7
C1.4 / 26.2	C1.1 / 25.2
C1.1 / 25.6	C0.7 / 24.6
C0.9 / 25.8	C0.8 / 24.8
C0.6 / 25.2	C0.4 / 24.2
C0.1 / 24.6	C0.0 / 23.6

F3.7 / 21.5	F2.7 / 22.5
F1.7 / 21.1	F1.4 / 22.1
C4.2 / 29.9	C4.7 / 30.9
C2.4 / 29.2	C2.6 / 28.2
C0.9 / 24.9	C1.1 / 25.9
C0.9 / 24.9	C1.1 / 25.9
C0.8 / 24.8	C0.9 / 25.8
C0.2 / 23.9	C0.4 / 24.9

Ditch Grades

New BM	0.64	1235.83			1235.19
New BM	4.69	1236.71	3.81	1232.02	
Culvert Fl.			8.16	1228.55	
264			8.26		
263			8.36		
262			8.46		
261			8.56		
260			8.66	1228.05	
	4.63	1237.18	4.16	1232.55	
259			9.23	1227.95	
258			9.33		
257			9.43		
256			9.53		
255			9.63		
254			9.73		
			9.60		1223.54

X in NW ¼ of W headwall at Sta 265+00

		℄
C 3.5	-.5	5.15
C 2.0		
C 3.5	-.4	4.5
C 4.5		
C 4.5		
C 4.5		
C 4.5	-.8	4.8
C 4.5		

Checking Slopes and Reset
9/25/2

New BM	6.88	1271.96			1265.08	
126			2.39	1269.57		
127			1.76	1270.20		
	5.02	1274.65	2.33	1269.63		
128			4.25	1270.40		
129			4.05	1270.60		
130			3.85	1270.80		
131			3.65	1271.00		
132			3.45	1271.20		
	7.25	1277.35	4.55	1270.10		
133			5.90	1271.45		
134			5.30	1272.05		
135			4.35	1273.00		
136			3.35	1274.00		
137			2.35	1275.00		

F1.0 / 23.1	F0.9 / 23.1	F1.5 / 22.7	F1.5 / 22.7
—	F0.8 / 23.4	F1.4 / 22.8	—
—	F0.8 / 23.1	F1.3 / 22.8	—
—	F0.1 / 24.5	F0.4 / 23.7	—
—	F0.9 / 23.0	F1.0 / 23.1	—
F1.2 / 22.7	—	—	—
F1.3 / 22.7	—	—	—
—	—	—	—
—	—	—	—
—	—	—	—
—	—	—	—
—	—	—	—
—	—	—	—

		1277.35				
	5.36	1281.46	1.25	1276.10		
138			5.46	1276.00	✓ ✓	
139			4.46	1277.00	✓ ✓	
140			3.58	1277.88	✓ ✓	
141			3.58	1277.88	✓ ✓	F0.8 / 23.1
142			4.46	1277.00	✓ ✓	F0.7 / 23.3
New BM	2.54	1279.63	4.20	1277.26	1277.09	
143			3.63	1276.00	✓ ✓	
144				No Shots X road		
145			5.00	1274.63	✓ ✓	
146			5.38	1274.25	✓ ✓	
	3.14	1276.77	6.00	1273.63		
147			2.89	1273.88	✓ ✓	F1.0 / 23.1
148			3.27	1273.50		
BM #14			4.11	1272.66	1272.70	
149						
150						

F0.2 / 23.9

F0.3 / 24.7

24.7

Checking & Resetting Slopes
9/26/29 Richey Rand.

BM#14	3.22	1275.92		1272.70	
149			2.79	1273.13	F1.8 / 22.1
150			3.17	1272.75	F1.4 / 22.5
151			3.54	1272.38	
152			4.11	1271.81	
153			5.03	1270.89	
	1.91	1271.70	6.13	1269.79	
154			1.92	1269.78	
155			3.03	1268.67	
156			4.01	1267.69	F1.6 / 22.1
157			4.10	1267.60	F1.4 / 22.7
158			3.29	1268.41	
BM#15	6.56	1274.95	3.23	1268.47	1268.39
159			5.60	1269.35	
160			4.66	1270.29	F1.2 / 22.8 — C0.4 / 24.9

	1274.95				
161		3.72	1271.23	F1.8 / 22.1	F0.4 / 24.0
162		2.78	1272.17	F2.2 / 21.2	F1.0 / 22.7
163		1.84	1273.11		F1.1 / 22.7
		1.82	1273.13		
164		[illegible]	1274.05		
165					

9/30/29 Richey Rand — Checking and Resetting Slopes

BM new	2.04	1278.61			1276.57		
164			4.56	1274.05	✓ ✓		
165			4.16	1274.45	✓ ✓	F0.2 / 24.3	C0.8 / 25.9
	3.58	1277.33	4.86	1273.75			
166			3.61	1273.72	✓ ✓	C0.0 / 24.3	
167			4.45	1272.88	✓ ✓	F1.4 / 22.4	F0.2 / 24.5
168			4.43	1272.90	✓ ✓	F3.3 / 20.9	F1.6 / 22.4
169			3.53	1273.80	✓ ✓	F2.2 / 21.5	
	9.95	1286.25	1.03	1276.30			
170			10.66	1275.59		C2.1 / 27.4	C0.7 / 25.1
BM #6	2.80	1286.32	2.80	1283.45	1283.52		
171			8.07	1278.25	✓ ✓	C2.5 / 28.2	
172			5.06	1281.26	✓ ✓		
173			2.71	1283.61	✓ ✓		
	4.42	1289.87	0.87	1285.45			
174			4.65	1285.22	✓ ✓		

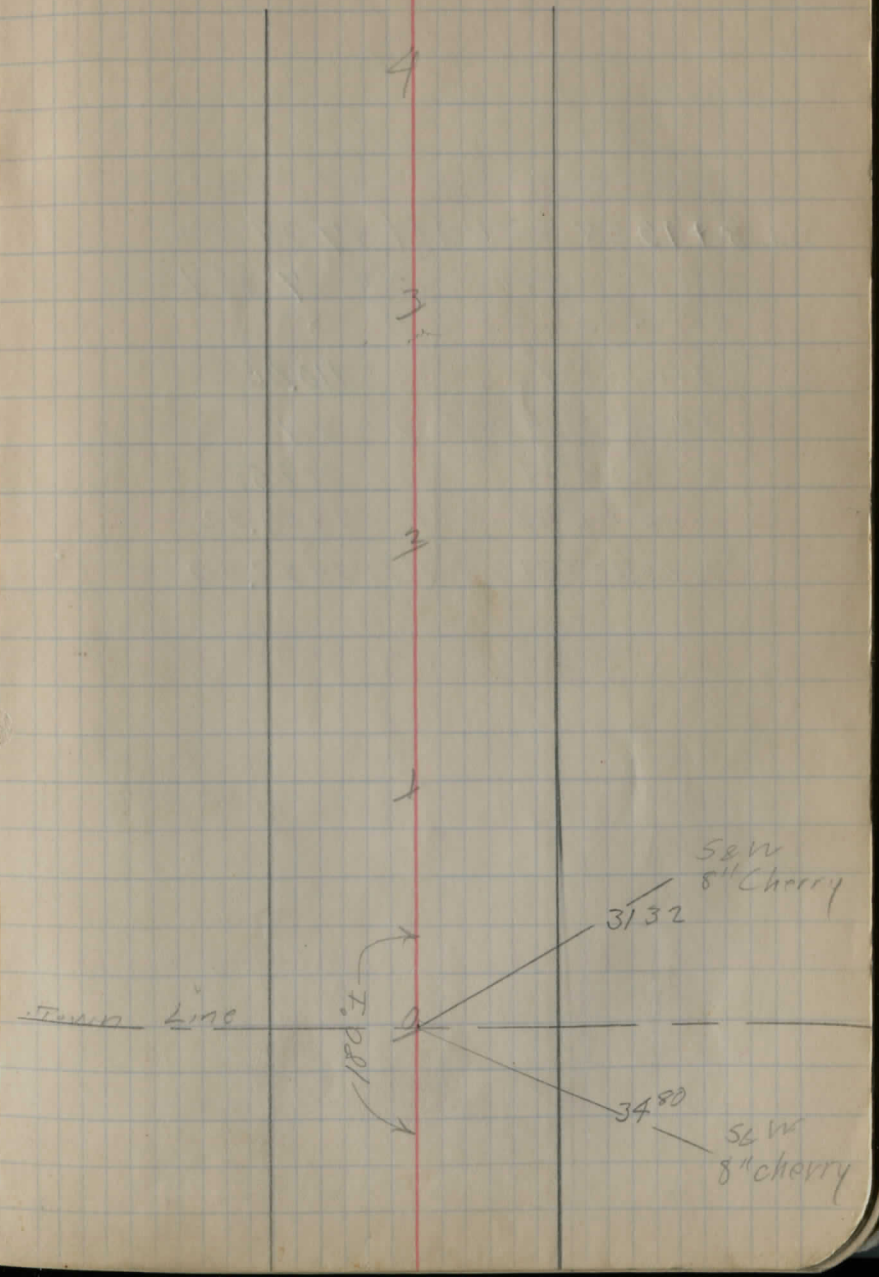
	1289.87			
175		3.78	1286.09	⌐ ⌐
176		3.57	1286.30	⌐ ⌐
177		3.50	1286.37	⌐ ⌐
178		3.31	1286.06	⌐ ⌐
179		4.50	1285.37	⌐ ⌐
180		5.25	1284.62	⌐ ⌐
New B.M.		5.60	1284.27	1284.26

12/12/30 Richey Barton Merrill

T.H. 211 Grove Road Location
Parkman Twp.

Sidestakes are set 25' Right or S.

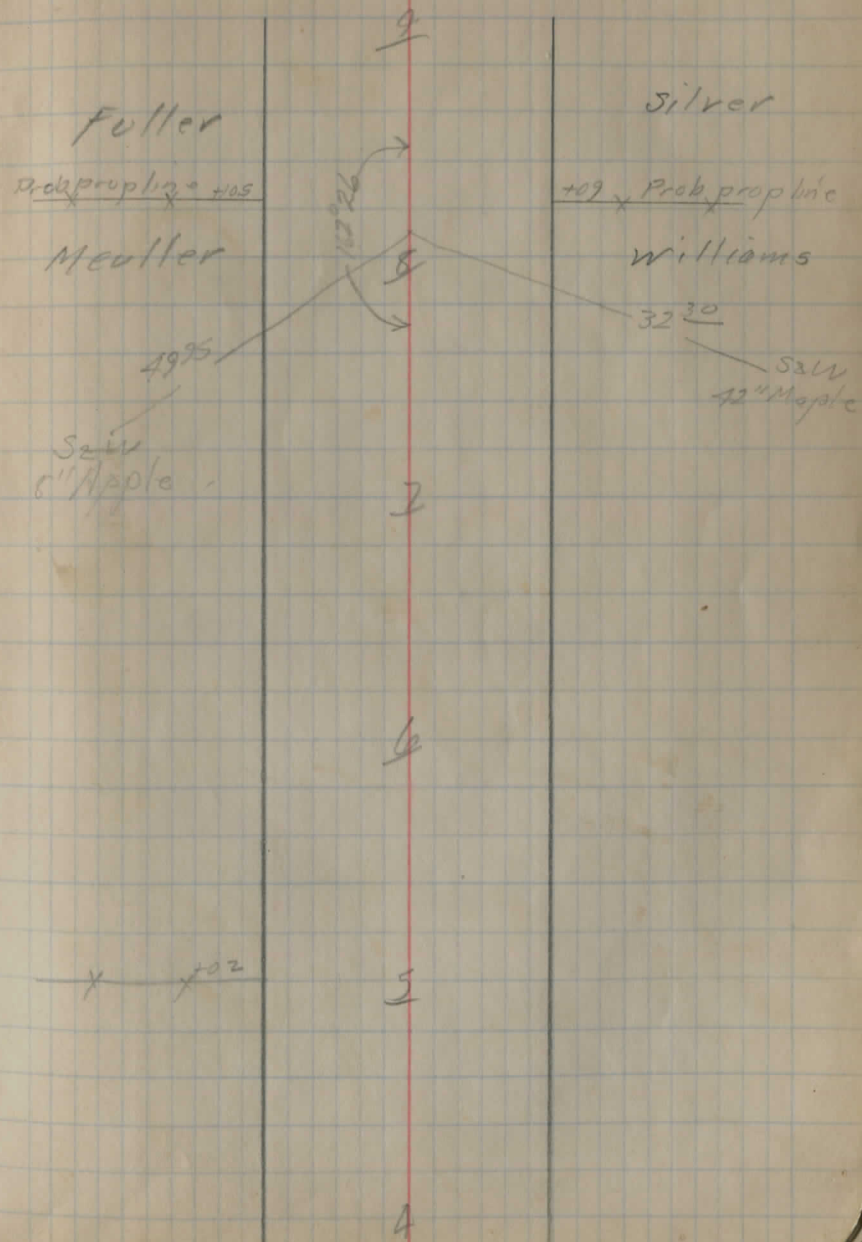
0+00 Beginning of Imp. Iron Set



Sta 8+13.58 Defl Lt 17°34' Iron set

Station	Deflection
9+22.5	0°00
9+00	0°54
8+50	2°54
8+00	4°54
7+50	6°54
7+02.92	8°47

Curve Data
- Δ = 17°34' L
- D = 8°
- T = 110.66
- E = 8.4
- L = 219.58
- PC = 7+02.92
- PT = 9+22.50



15

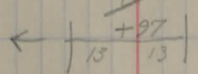
14

13

12

11

80° Lt Fd
4 x 3 slab Top.
masonry wall
balance is std Conc



10

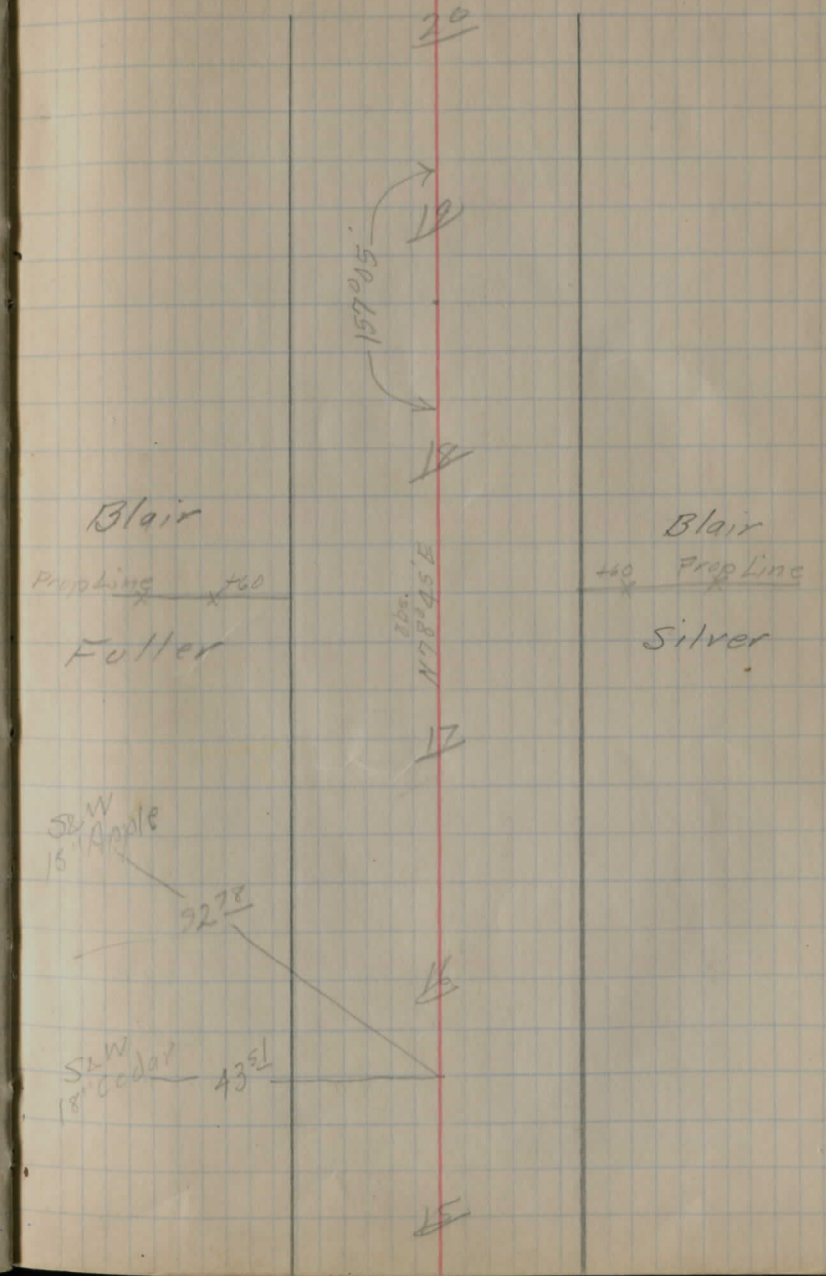
9

Sta 18+69.00 Def Lt. 22°55 From Set

Curve Data
- Δ = 22°55' Lt
- D = 9°30'
- T = 258.07
- E = 25.9
- L = 508.26
- PC = 16+1093
- PT = 21+1319

21+1319	= 0°00
21+00	= 0°26
20+50	=
20+00	= 3°41'
19+50	=
19+00	= 4°56
18+50	=
18+10	= 7°11
17+50	=
17+00	= 9°26
16+56	=
16+1093	= 11°27

Sta 15+71.70 POT From Set



25

24

10" Cor I P, in
poor condition ← +85 / 14 9

+85 × ×

23

+06 × ×

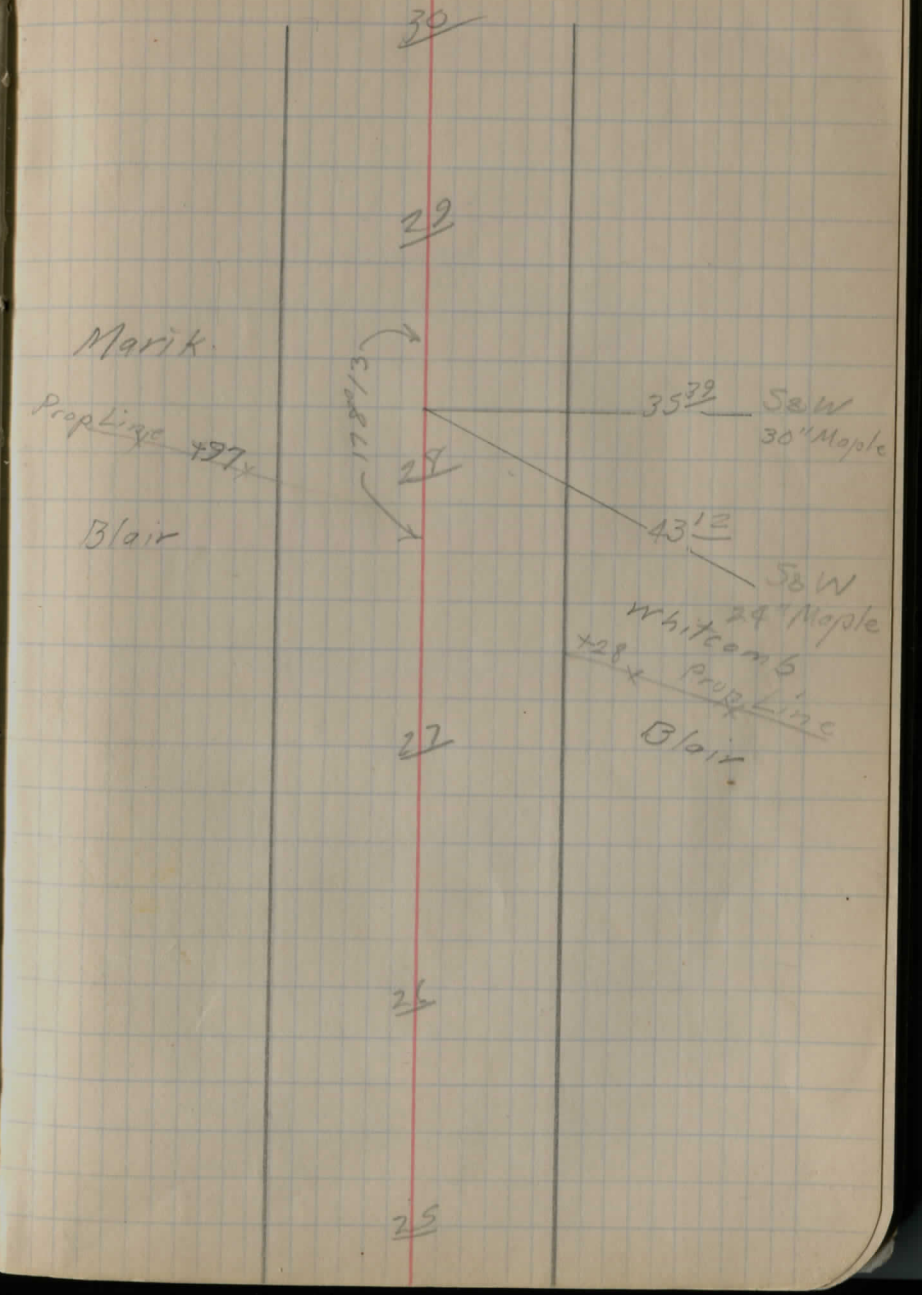
22

4 X 3 Slab Top
masonry walls
Std conc tops
wings
in good condition ← +23 / 125 135

21

20

Sta 28+16.00 Def Lt. 1°47' Iron set



35

34

33

Marik

+28 Prop Line

Whitcomb

32

80° Rt Fd.
10" Cor I P
in fair
condition

+59
4 16

31

30

40

39

38

+19

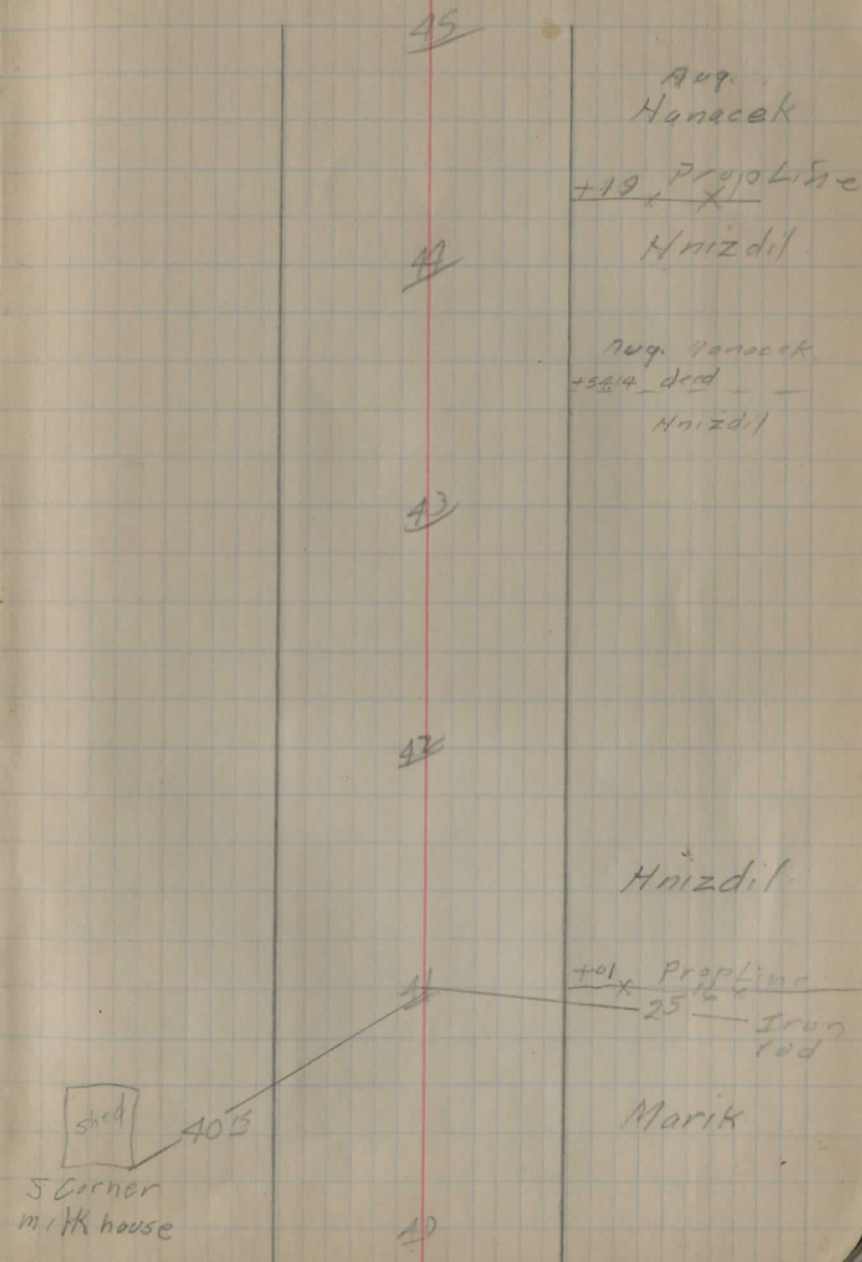
15" Cor I P in
good condition ← +24.5 7 10
conc headwalls

37

36

35

Sta 41+00.69 | POT | spike Set



50

49

48

Anton Hanacek.

+16.16 deed

Aug. Hanacek

47

15" Cor I P in
glodcondition
conc headwalls

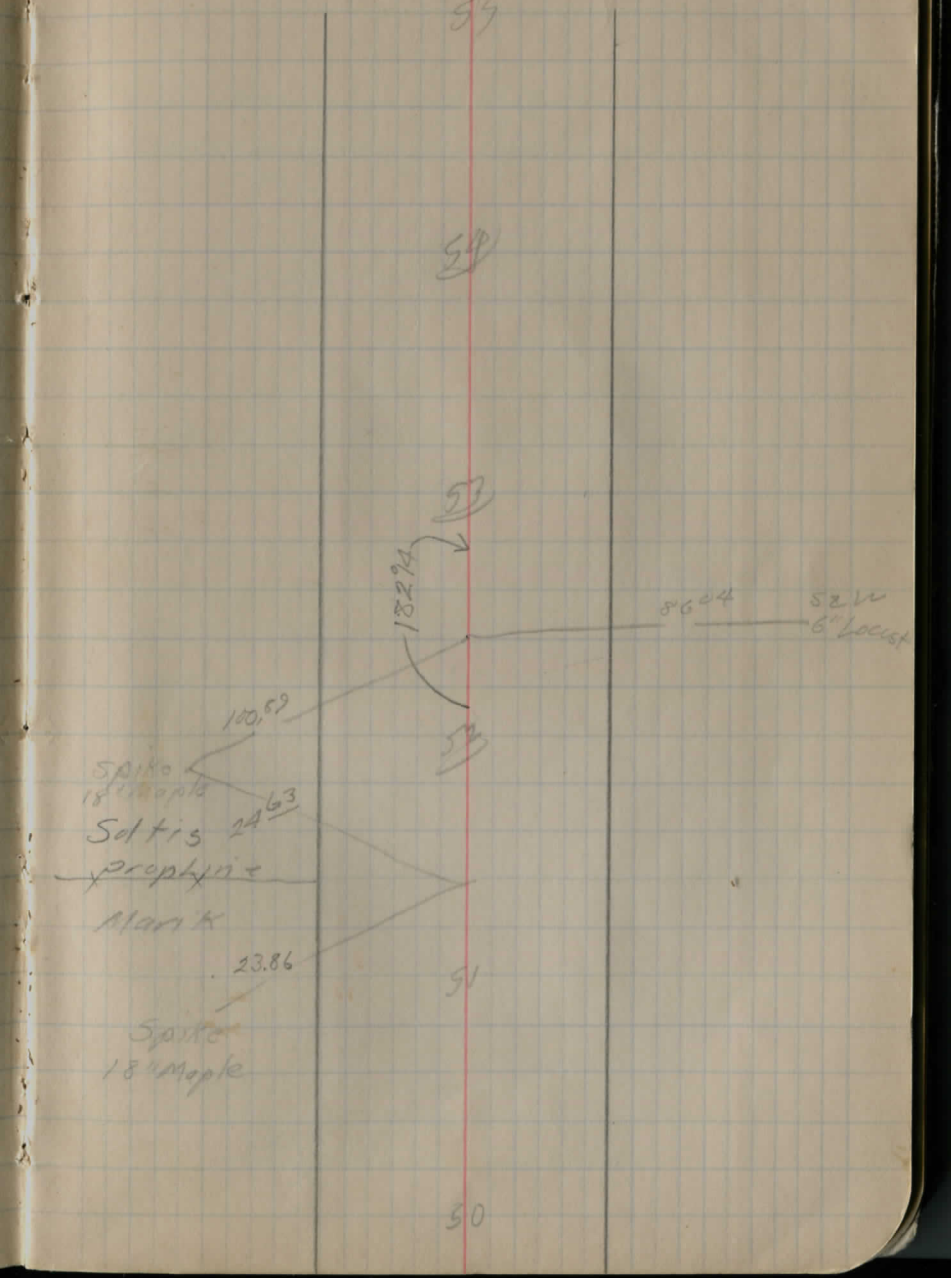
← 4+55
9 8

46

45

Sta 52+46.98 Det Rt 2°14' Iron Set

Sta 51+36.26 PDT Iron Set



12" VSP Conc. headwalls in good condition

← +58 | 12 | 7

60

59

58

Aug. Hanacek.

+14 Possible prop line

Anton Hanacek.

57

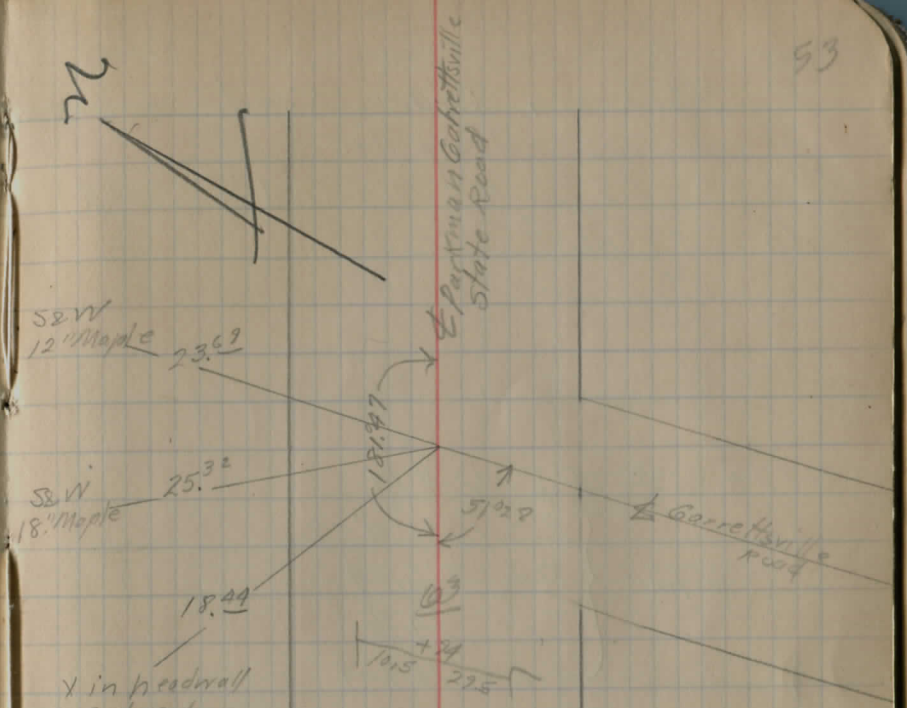
56

55

1.194 miles

5280 | 6305
5280
1025
5280
4970
4752
218

Sta 63+18.32
Edge of Pvt 63+05



5 Gold
3 Morrill
H Barton

Parkman Grove Road. ℄ Location

Troy Twp.

Sta 25+25 ℄ Mumford Cors Road

Sta 24+00 P.O.T.

Sta 17+70± P.I. Def Lt.

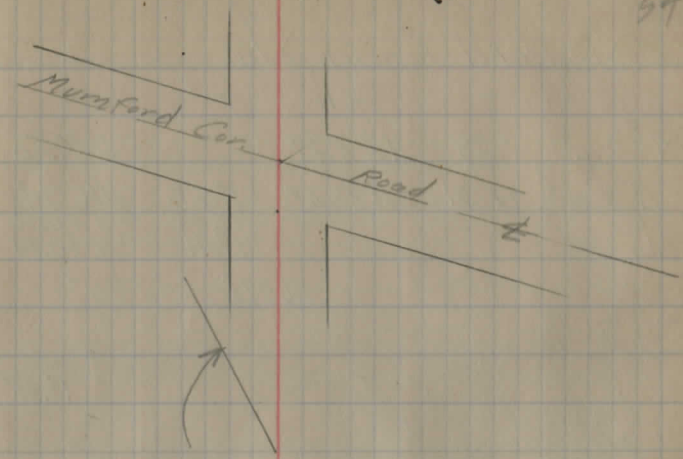
Curve Data
- Δ = 15°00'
- R = 716.74
- Tan = 94.36
- Arc = 187.69

Sta 11+00 POT Iron Set

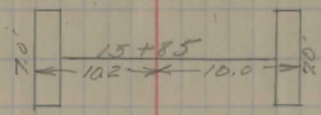
Sta 0+00 Iron Set

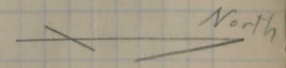
GROVE RD #211 SEC. 0 (pt.)

54



3'x4' Stone Box culvert in good condition





Troy Twp. / Parkman Twp. — Twp Line

4/24/40 Pomeroy - Richards

Windy 50°

55

Mumford Road Sta.

	+	H.I.	−	E	to
BM #3a	1.69	1122.77		1120.00	
T.P.	12.31	1128.25	5.83	1116.94	
E. E.L.			17.55	1110.70	
W. F.L.			19.41	1110.84	

36+78

37+0 Ocreek 18.35

38+0 21.85

39+0 24.45

40+0 26.45

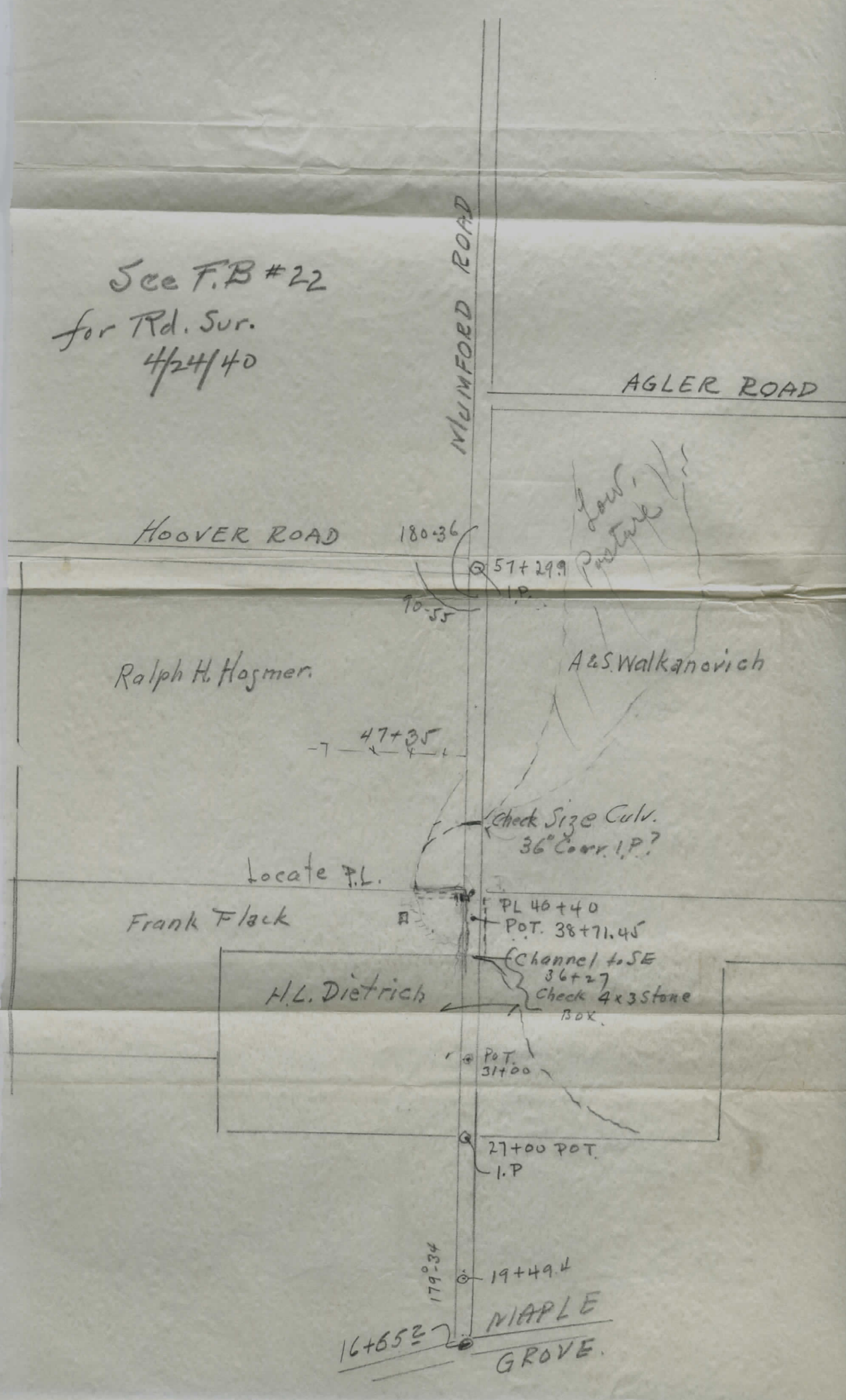
+36 Drive both sides
+44 channel
+49.5 P.L's 26.25

E. Rot 24" Map. 60' Lt Sta 31+10
S.W. cor. West Hdwl Culv't Sta 36+28
4.5'x3'x39 Conc Culv't. Conc. floor. Skewed
Skewed.

	W									E
(15.5)	13.1	12.7	12.1	11.6	10.4	9.9	10.4	11.3	9.4	2.1
60	55	45	30	18	16	E	15	14 17	20	32
(12.8)	9.8	9.4	8.3	8.1	7.0	6.4	6.7	7.5	5.9	+1.0
28 32	25	23	21	18	16	E	16	18	21	32
(10.7)	8.1	7.7	4.4	4.3	5.5	4.4	3.3	4.1	4.5	+3.7
47	44	38	31	21	18 19	15	E	15.5	17 19	32
(8.2)	6.3	3.8	2.0	1.8	2.2	2.6	+3.7			
31	28	20	14	E	18	19	30			

24.65

2.2	2.9	3.6					
± 190	± 150	20 Bridge	E				
4.9	5.2	5.8	1.7	1.4	1.2	1.9	+3.3
30	25	20	14	E	15	18 19	30


See F.B #22
for Rd. Sur.
4/24/40
MILLFORD ROAD
AGLER ROAD
HOOVER ROAD
180-36
51+29.9
I.P.
90-55
Low Pasture
Ralph H. Hosmer
A&S. Walkanovich
47+35
Check Size Culv.
36" Corr. I.P.?
Locate P.L.
Frank Flack
PL 46+40
POT. 38+71.45
Channel to SE
36+27
Check 4x3 Stone
Box.
H.L. Dietrich
POT.
31+00
27+00 POT.
I.P
179-34
19+49.4
MAPLE
GROVE.
16+65±

		1122.25		
40 of 44	+	H. I.	-	Elev
T.P.	7.49	1133.83	1.91	1126.34
41 to				27.23
+10				
42 to				28.73
43 to				30.33
+45	36"x	Enc Corr. I.P. Culvt - skewed		
T.P.	0.08	1133.83	9.14	1124.69
B.M.		1125.77	8.8.5	1116.92
TP		1125.77	12.21	1113.56
T.P.	10.07	1123.63		
BM #32			2.78	1120.85

W E

5.3 7.9
± 150 20 E

13.1 9.5 6.4 5.6
So. P.L. 300 100' 10' S of Dr
S of Dr. S. of Dr. 190' back

N W. & W. Hdwl Sta 41+10
12"x Enc. V.S.P. Culvt

9.7 9.1 8.3 7.3 6.6 7.1 9.1 7.0
30 25 20 15 E 19 23 30
24

~~33~~.13 23.83
10.7 10.0
F.L. F.L.

6.7 7.9 5.5 5.1 5.7 8.5 6.6 6.9
25 20 15 E 14 19 23 30
30 20

5.6 6.0 3.8 3.5 3.8 6.4 4.5 4.4
25 20 14 E 12 17 25 30
30 20

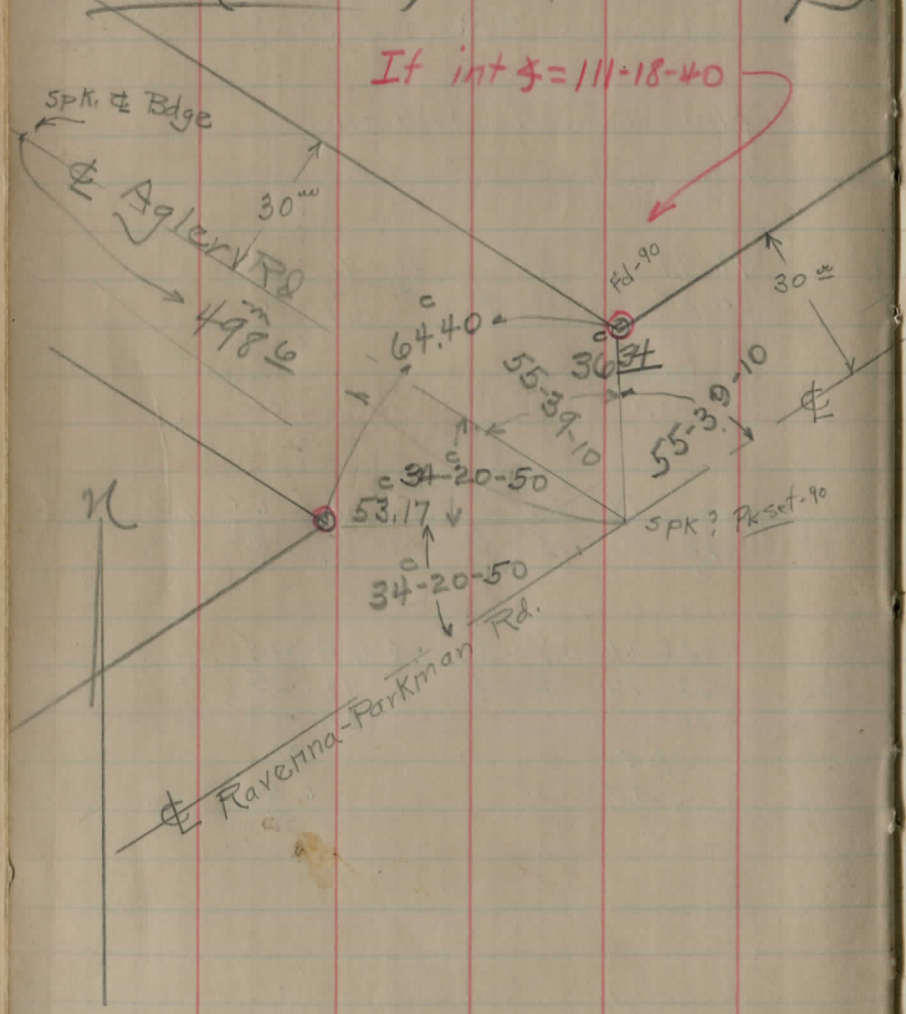
27.4 27.3
6.45 6.54
F.L. F.L.

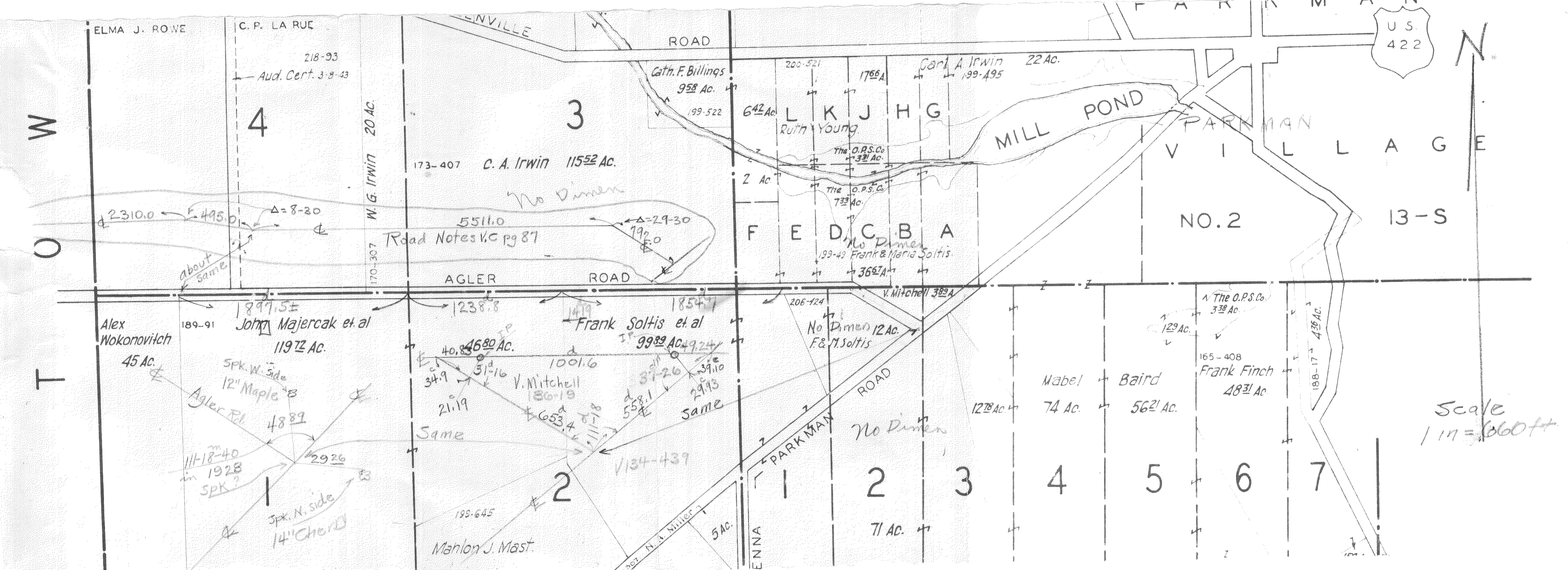
S.W. Cor. W. Headwall Sta 36+28

Agler (CH #210) E. end Parkman Twp.

See pg. 53 (this book) Interstn Grove Rd & Route 88

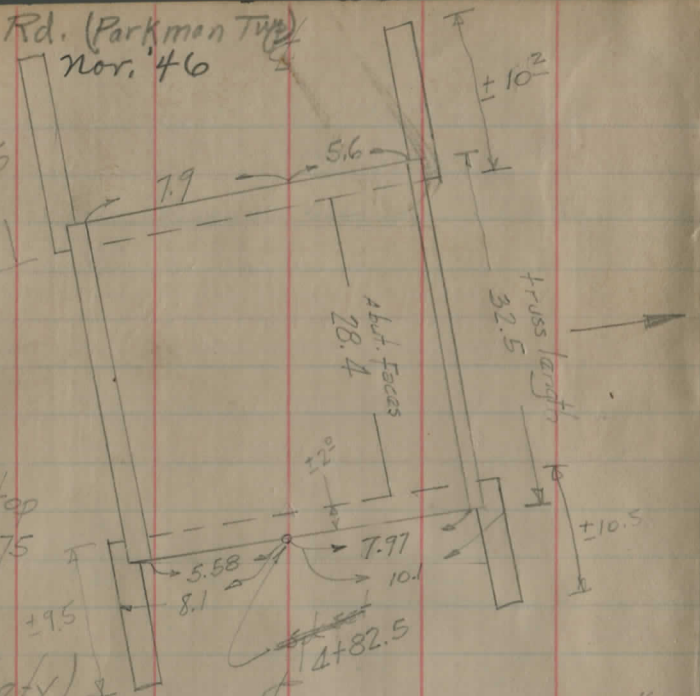
Route 88 (ICH. 326) is monumented on N/W/y.





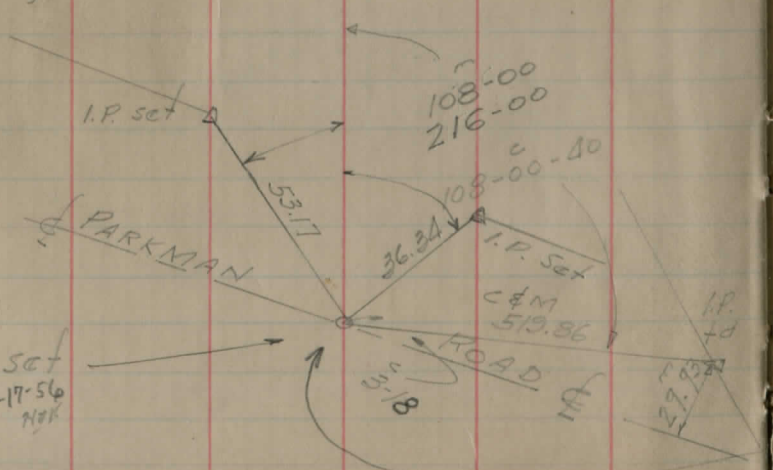
ELMA J. ROWE
C. P. LA RUE
218-93
Aud. Cert. 3-8-43
4
W. G. Irwin 20 Ac.
3
173-407 C. A. Irwin 115.52 Ac.
No Dimen
ROAD
Cath. F. Billings 9.58 Ac.
199-522
200-521
17.66 A.
Carl A. Irwin 22 Ac.
199-495
6.42 Ac.
L K J H G
Ruth Young
The O.P.S. Co 3.31 Ac.
2 Ac.
The O.P.S. Co 7.33 Ac.
MILL POND
PARKMAN
V I L L A G E
U.S. 422
N
NO. 2
13-S
F E D C B A
No Dimen
199-49 Frank & Maria Soltis
36.67 A.
2310.0
495.0
Δ=8-30
5511.0
Δ=29-30
Road Notes V.C pg 87
about same
170-307
AGLER ROAD
1897.5±
1238.8
1419
1854
V. Mitchell 3.89 A.
206-424
Alex Wokonovitch 45 Ac.
189-91
John Majercak et al 119.72 Ac.
Frank Soltis et al 99.89 Ac.
49.24
No Dimen 12 Ac.
F. & M. Soltis
The O.P.S. Co 3.38 Ac.
12.9 Ac.
165-408
Frank Finch 48.31 Ac.
188-17
43.6 Ac.
40.83
46.80 Ac.
1001.6
34.9
31-16
V. Mitchell
186-19
653.4
558.1
37-26
39.10
29.13
Same
21.19
Spk. W. Side
12" Maple
Agler Rd.
48.89
29.26
111-18-40
in 1928
Spk?
Same
V134-439
PARKMAN ROAD
No Dimen
Mabel 74 Ac.
Baird 56.21 Ac.
12.78 Ac.
Scale
1 in = 660 ft
1
2
199-645
Spk. N. side
14" Cherry
Manlon J. Mast
N. A. Miller
5 Ac.
ENNA
1 2 3 4 5 6 7
71 Ac.
T O W

Agler Rd. (Parkman Twp.)
Nov. '46



truss ht
floor to top
truss : 37.5

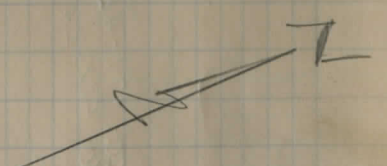
(Variety) Iron Wks.
Iron lattice girder brdge 5-I beam ±8"
longit. stringers 1-Ibeam ±12" transverse
stringer

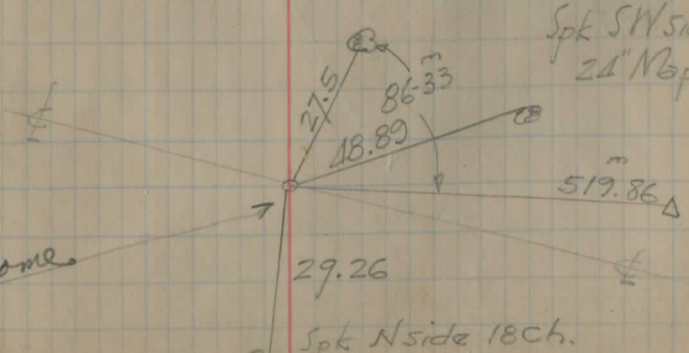


57

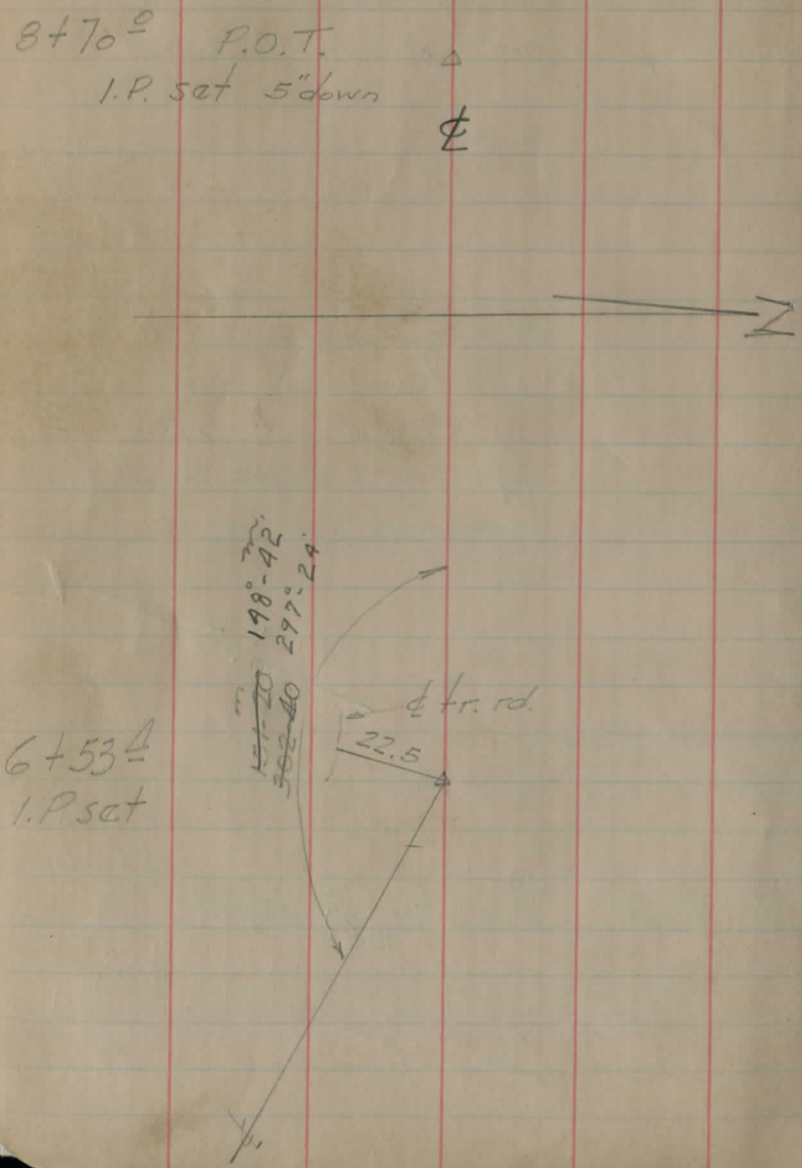
± clear ht = 11.1
Stone abut. in fine shape
plank flooring ± 5' needs re-
placing immediately 14' lengths

Stakes set 30' Lt
Every sta. 1-8 inc!
8 on = each 200'
Sta 44+0 & west = 30' Rt



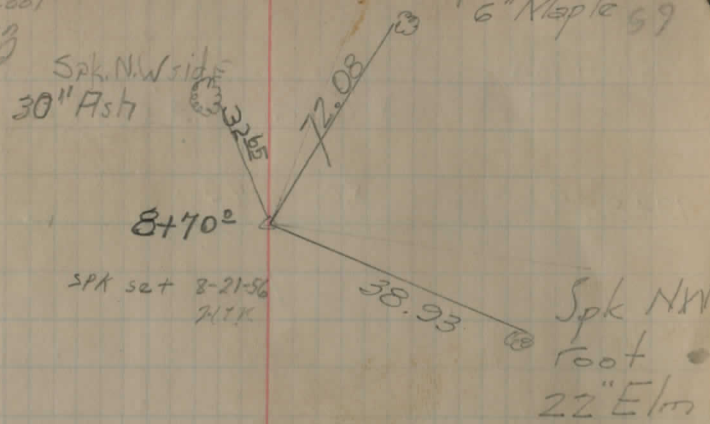


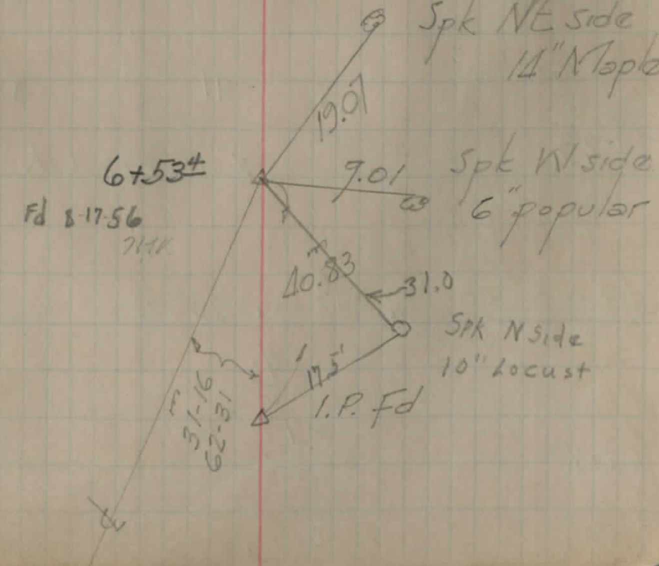
Agler Rd



Aug 21, 1956
Clear + Cool
Patterson
Canfield
Rafie

69





22+0 Agler Rd.

21 — 21

8" Corr. ℄ ± 3' C.I.P. on N end OK

19+82.8 — 8.0 | 11.3

℄

8+23.7 line spk

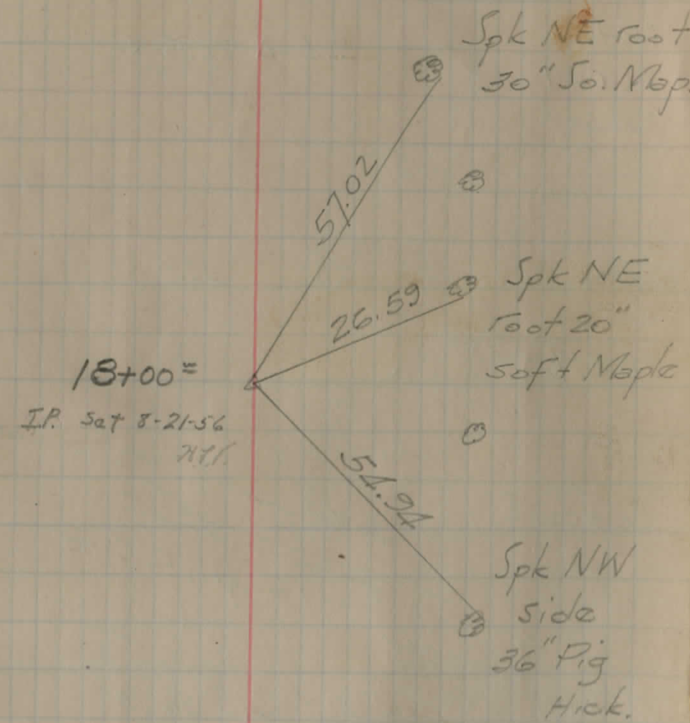
18+00.0 P.O.T. I.P. set — 22' | 20.5

16+08 — Irwin / Soltis

15+23 — 8.8 | 9.1 — 8" Corr. OK

14+0 — 17.5 | 20.0 — ℄

10+08 — 5.4 | 10.7 — 10" Corr. OK



Agler Rd.

42+00 — 20.3 — 22.5

38+00 P.O.T. I.P. set — 22.5 — 22.5

34+00 — 23.8 — 22.2

30+47 MAST SOLTIS

30+04 — 6" — 10" Corr. — 16" — 1 length 12" Conc.

30+00 — 27.3 — 20

26+00 — 25 — 22

22+71 — 9.0 — 7.2

12" Corr N6 (rusted out)

I.P. fd 8-30-54 M.H.I.

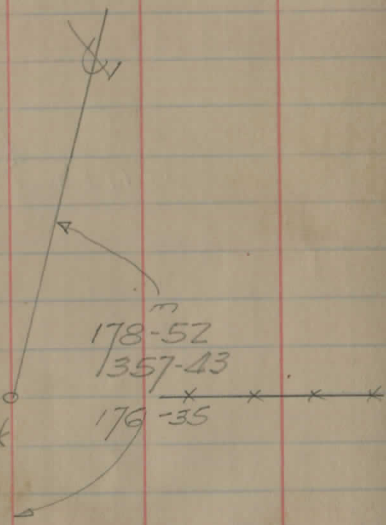
38.95 — Spk E side 16" Maple

36.05 — Spk SE side 12" beech

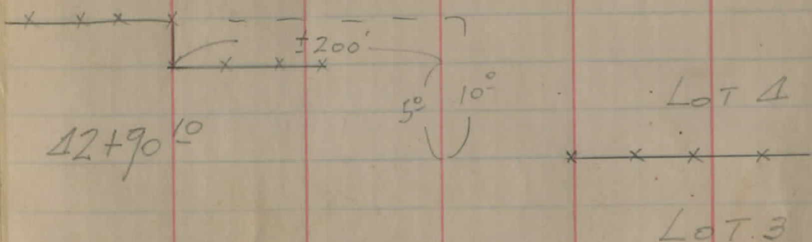
51.35 — Brock

Spk SE side 14" beech

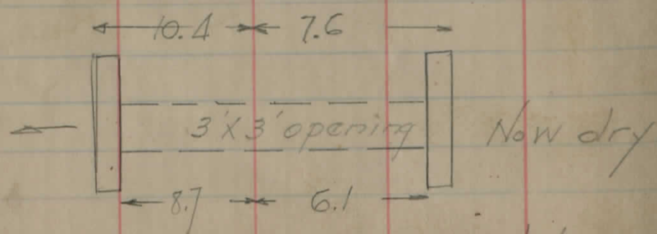
46+74.5 Spike in N wheel track



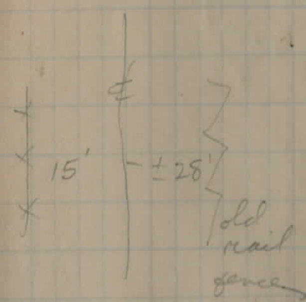
42+90.10

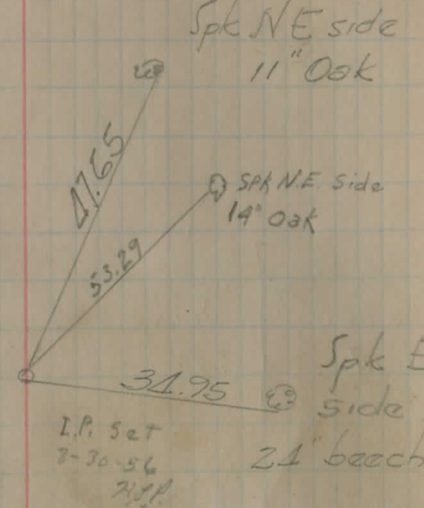


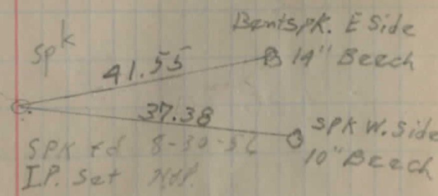
42+82.3



Fair shape Stone abut. Conc. slab
Stone rders







57 + 36⁵

House
56+00 38
P.O.T.

Spike

1° N of N wheel track

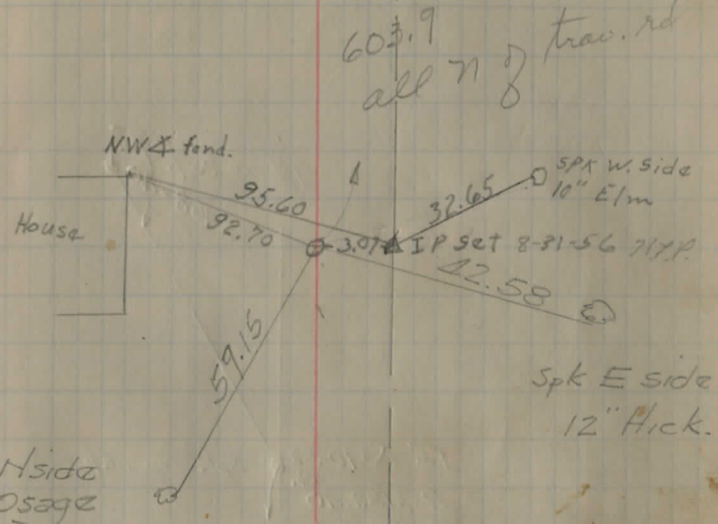
54+0 — 24 — Last stk

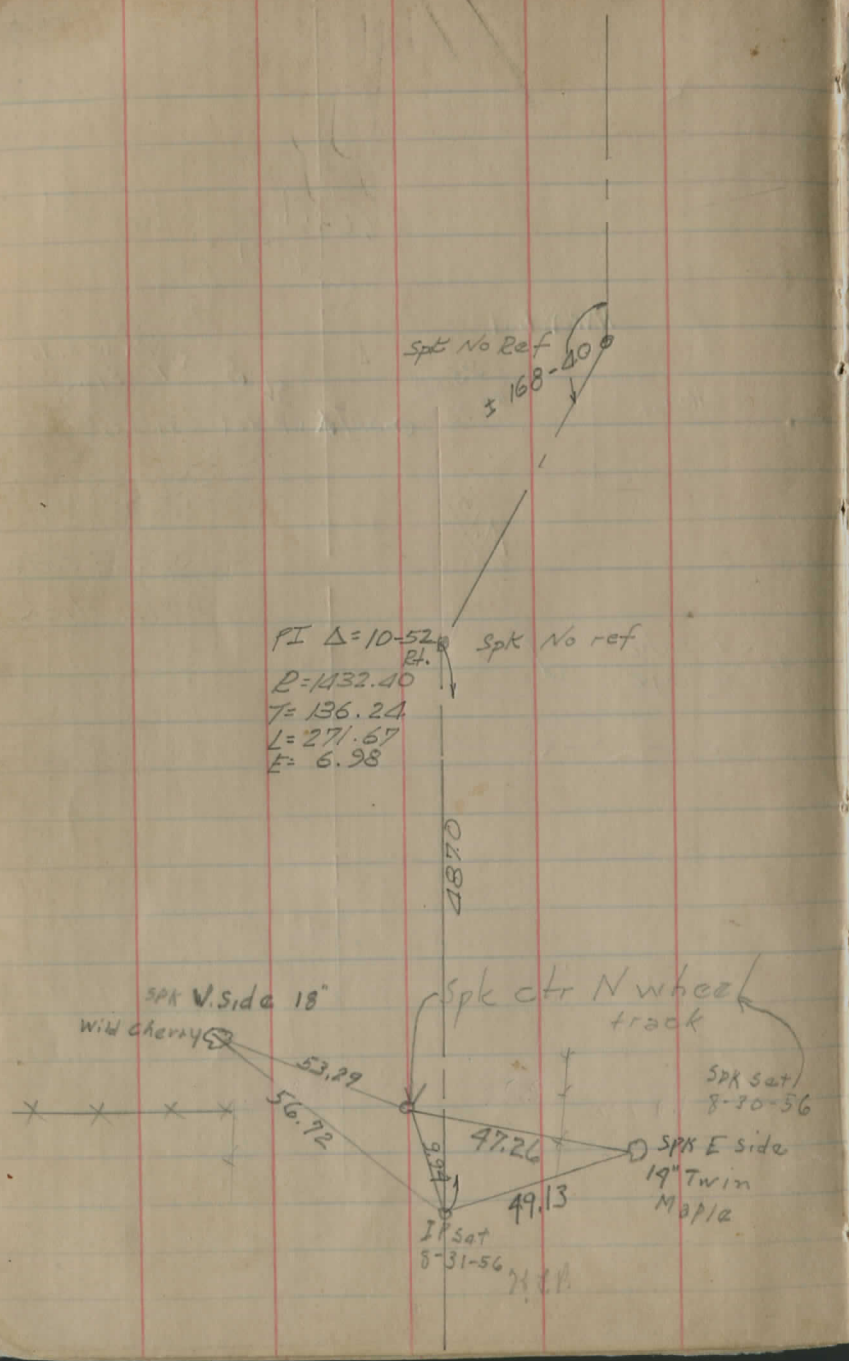
℄ Mast Drive

53 + 25

N edge tr. rd.

50+0 — 18 — 29.3





SUN MON TUE WED THU FR

1 2 3 4 5

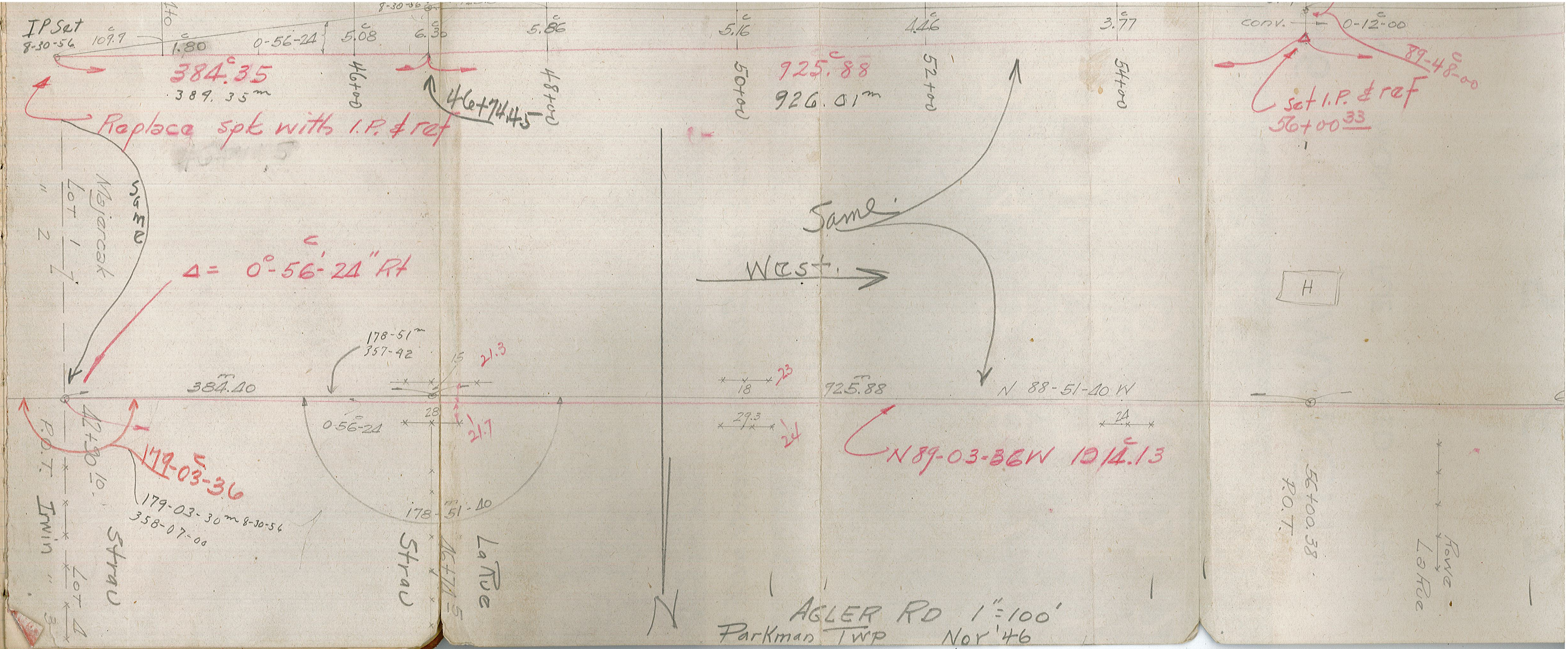
7 8 9 10 11 12

14 15 16 17 18 19

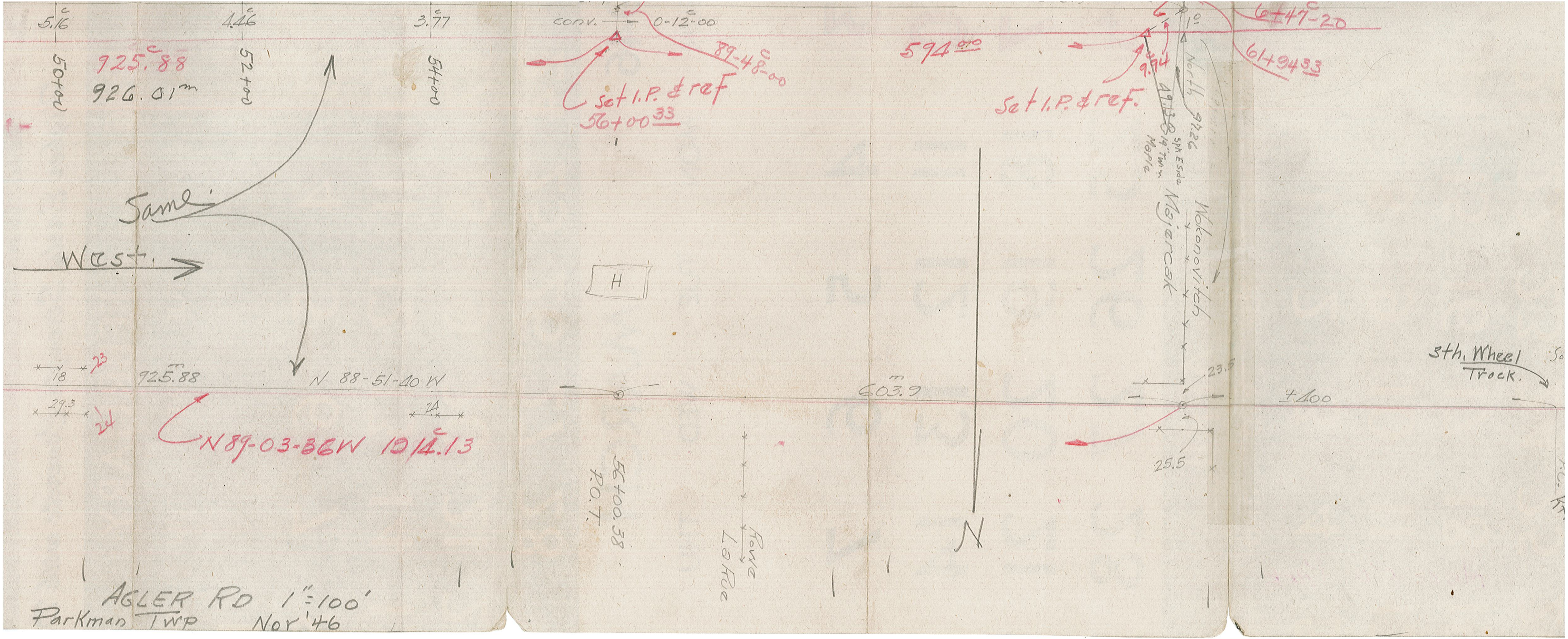
21 22 23 24 25 26

Access Rd Pack

Access Rd Pack



IP Set 8-30-56
109.7
1.80
0-56-24
5.08
6.30
5.86
5.16
4.46
3.77
conv.
0-12-00
384.35
389.35m
46+00
46+74.45
48+00
50+00
925.88
926.01m
52+00
54+00
89-48-00
Set I.P. & ref
56+00.33
Replace spk with I.P. & ref
Same
Majercak
Lot 1
Δ = 0°-56'-24" Rt
Same
West
H
178-51m
357-42
15
21.3
23
384.40
18
925.88
N 88-51-40 W
28
0-56-24
21.7
29.3
24
N 89-03-36 W 1014.13
42+30.10
P.O.T.
179-03-36
179-03-30m 8-30-56
358-07-00
178-51-40
Irwin
Lot
Strau
Strau
46+74.45
La Rue
N
AGLER RD 1" = 100'
Parkman Twp
Nov '46
56+00.38
P.O.T.
Rowe
La Rue


5.16
4.46
3.77
50+00
52+00
54+00
925.88
926.01m
conv.
0-12-00
89-48-00
Set I.P. & ref
56+00 33
594.00
Set I.P. & ref.
9.94
North
97.26
61+47-20
61+94 33
Same
West
H
18
23
925.88
N 88-51-40 W
29.3
24
24
N89-03-36W 1014.13
603.9
23.5
25.5
56+00.38
P.O.T.
Rowe
LaRue
N
Majercak
Wolonovitch
5th Wheel
Track.
AGLER RD 1"=100'
Parkman Twp
Nov '46

6/23/33

66

Bridge 150' W of Cider Mill 1 mile South and ½ mile W of Middlefield

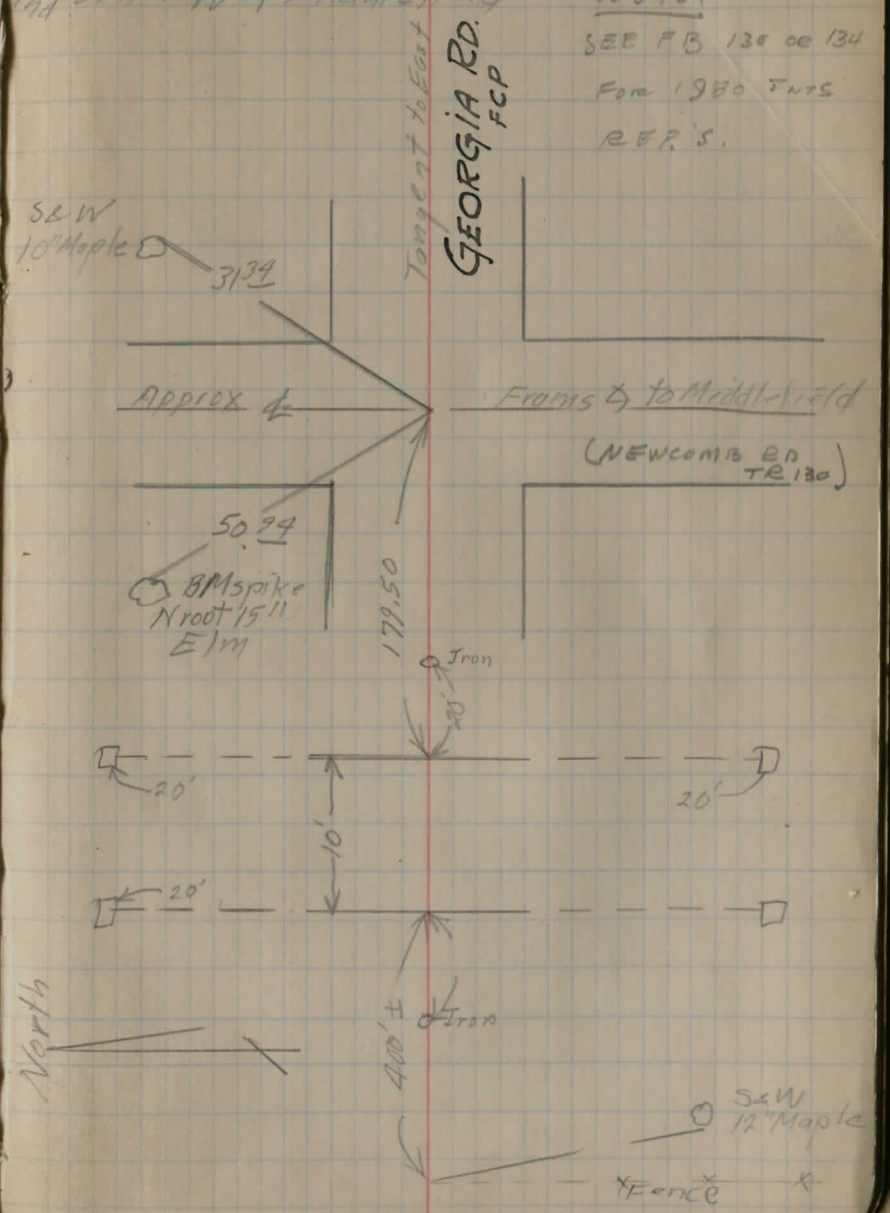
Cross Road — spike set

E Abutment

W Abutment

Angle in road — spike set

Notes:
SEE FB 130 or 134
For 1930 TNTS
R.E.P.'s.



6/23/33

67

Bridge @ 150' W of Cider Mill 1 mile S. ½ mile W of Middlefield

BM		3.25	103.25	Spike in root 15" Elm
100' E	Rod		3.8	99.4
Bridge E	"		5.1	98.1
" W	"		5.5	97.7
100' W			5.8	97.4

Grade on culvert Sta 123 + 24

BM	0.98	100.98		100.00	
℄ road			1.5	99.5	
old flow R.			13.2	87.8	8.0
" " L.			13.2	87.8	8.0
new flow R.			13.5	12.0	C1.5
" " L.			12.9	9.9	C3.0
Flow 50' R			13.6		
" 50' Lt.			11.4		

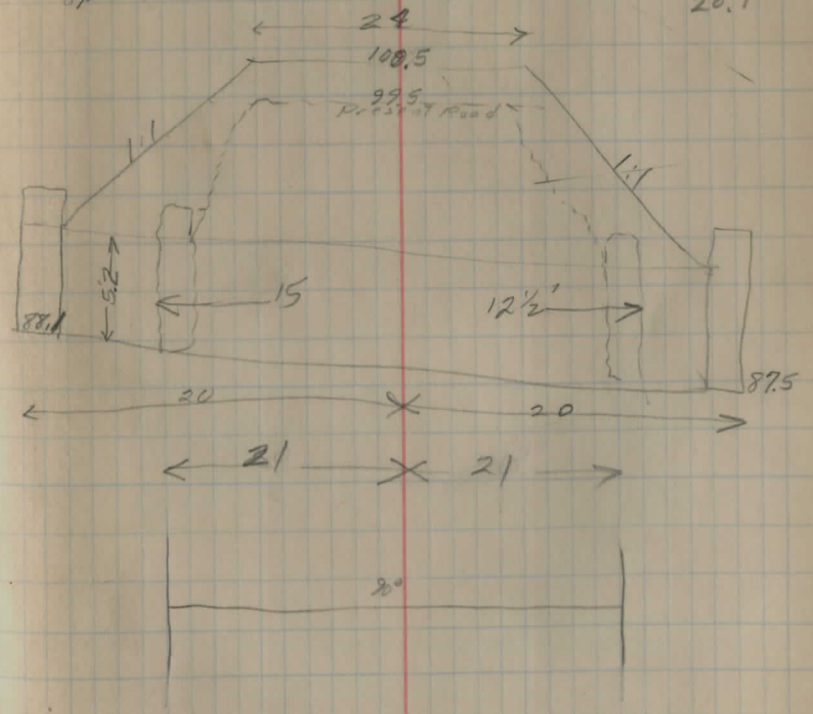
From 4s N Road
5 root 15" Maple 20' E of ℄ and 40' N of culvert

005
87.5
13.0
5.8
7.2
1.5
12.9
20.7

005
88.1
12.9
5.8
6.6
1.5 Road
12.0 Road
20.1

01.0
12.9
88.1

01.0
13.2
87.5



100 = 2.15
50 = 1-07-30
1 = 1.35

136

25807
45) 116 1.2
90
261
225
363
360
300

135
19
1215
135
2565

117 38
115 66
1.72

56
115 66
5) 116.52
23

5
9
50825
45) 22916666
225
416
405
116
90
266

1-26
2 15
2 41
2 15
4 56
2 15
7-11
2 15
9 26
2
121 27

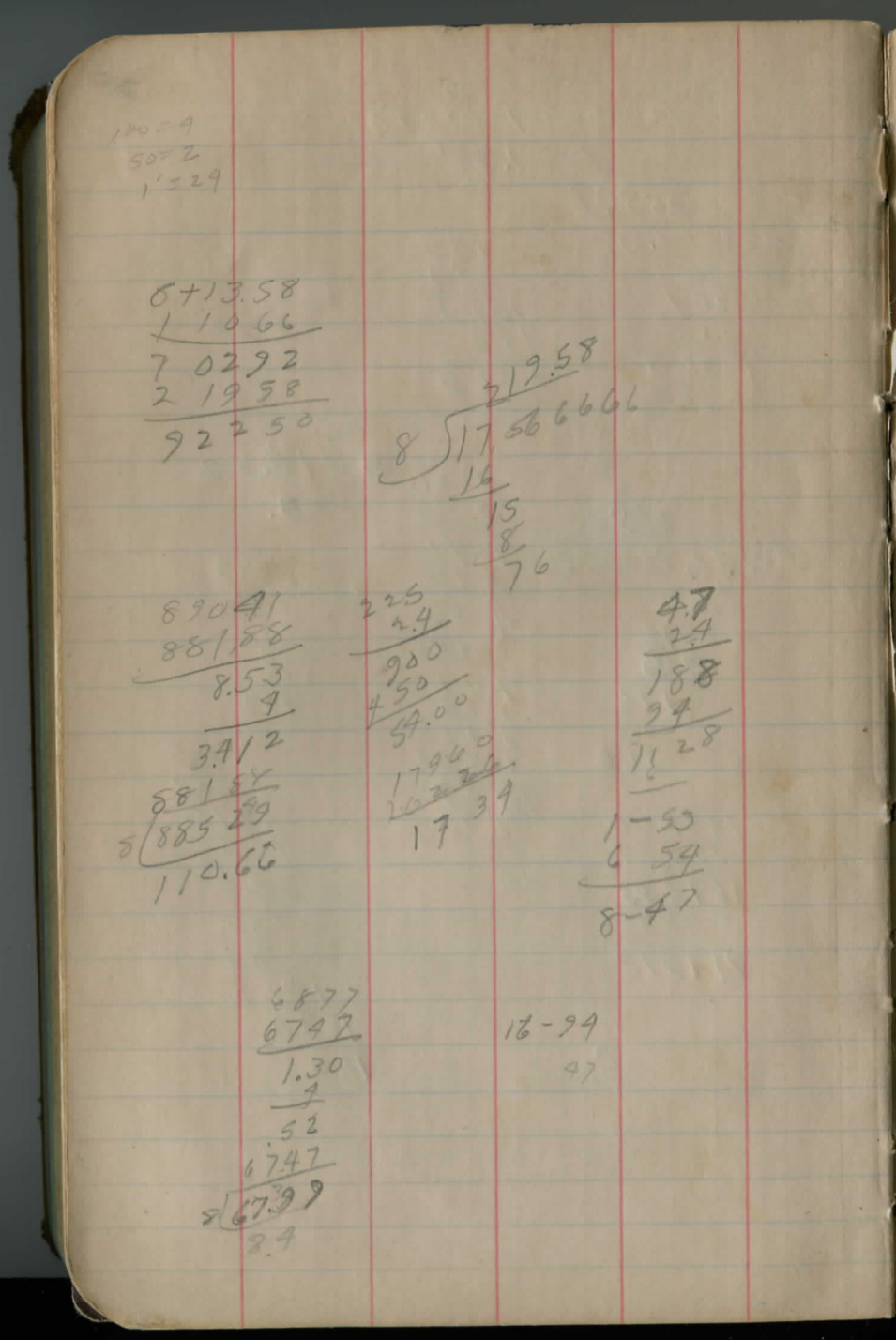
25.9
45) 116.52
90
265
225
402

135
38
1215
405
526

1869.00
258 07
161093
50826
211919

135
89
1215
1080
120

80.38
120

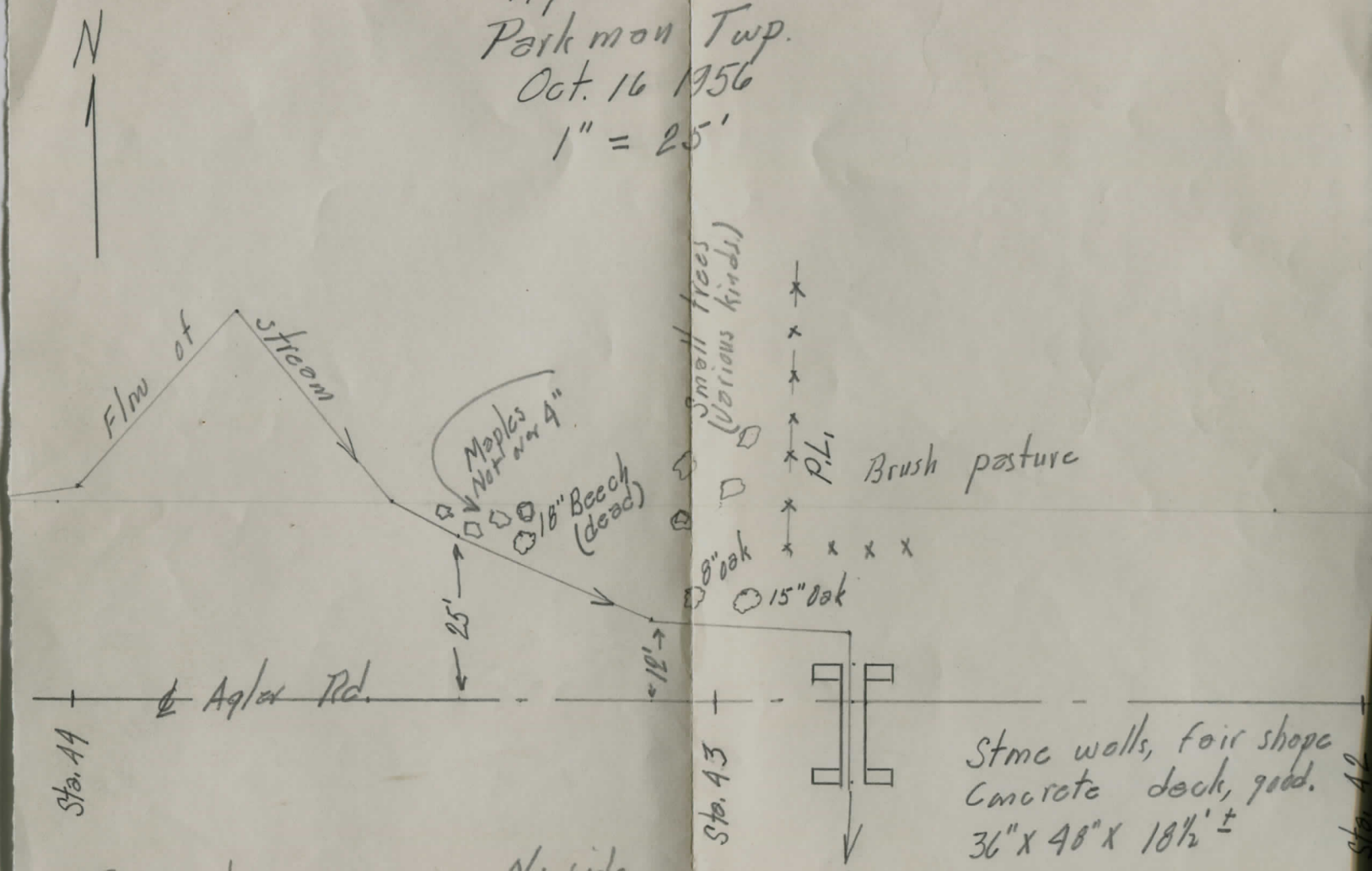


IMPROVED TABLES

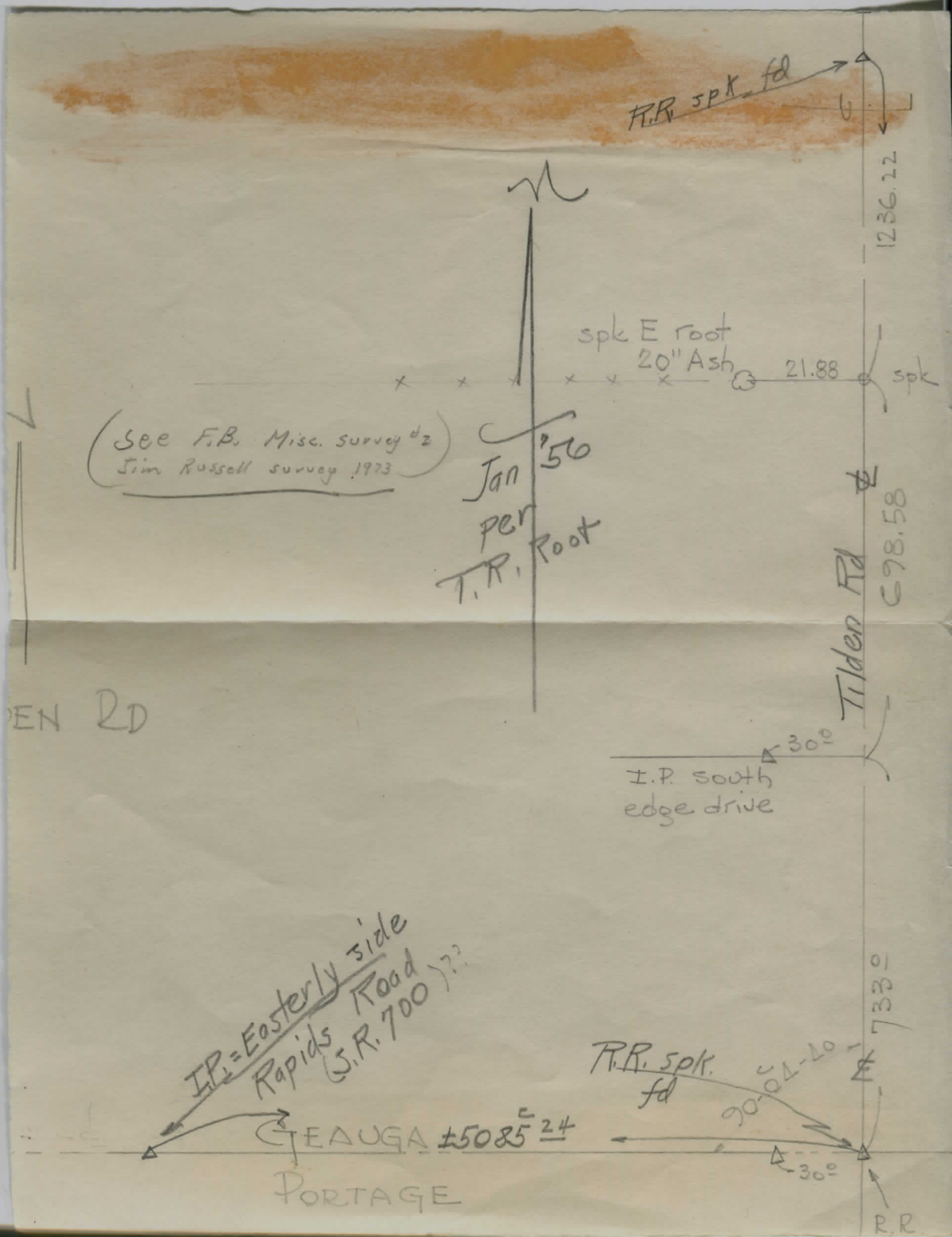
AND

INFORMATION

Drainage Problem
Agler Rd.
Parkman Twp.
Oct. 16 1956
1" = 25'



Property owner on No. side West of culvert claims no trees to be cut.


R.R. spk fd
1236.22
spk E root
20" Ash
21.88
spk
(See F.B. Misc. survey #2
Jim Russell survey 1973
Jan '56
per
T.R. Root
Tilden Rd
698.58
EN RD
30°
I.P. south
edge drive
I.P.=Easterly side
Rapids Road
(S.R. 700)??
7330
R.R. spk.
fd
90°04'-10"
GEAUGA ±5025' 24
30°
PORTAGE
R.R.